# BENCH-SCALE TREATABILITY TESTING REPORT

## **FINAL**

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Prepared for:

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#### LIST OF ACRONYMS

AOC Area of Concern

ASP Activated Sodium Persulfate
CAO Corrective Action Objective
COPC Chemical of Potential Concern

CSM Conceptual Site Model

DNAPL Dense Non-Aqueous Phase Liquid

DPE Dual-Phase Extraction

EDC 1,2-Dichloroethane (or Ethylene Dichloride)
EPA U.S. Environmental Protection Agency

FMC FMC Environmental Solutions FPC-TX Formosa Plastics Corporation, Texas

GPM Gallons Per Minute

ISCO In-situ Chemical Oxidation

ISOTEC In-Situ Oxidative Technologies, Inc.

mg/L Milligrams Per Liter
MPE Multi-Phase Extraction
ORP Oxidation-Reduction Po

ORP Oxidation-Reduction Potential
PBW Pastor, Behling & Wheeler, LLC
PCL Protective Concentration Level
RFI RCRA Facility Investigation
RMP Risk Management Plan
ROI Radius of Influence

SWMU Solid Waste Management Unit

SVE Soil Vapor Extraction
TDS Total Dissolved Solids
TOC Total Organic Carbon

TRRP Texas Risk Reduction Program

VCM Vinyl Chloride Monomer Process Area

VOCs Volatile Organic Compounds

WWTP Former Waste Water Treatment Plant

ZVI Zero-Valent Iron

#### 1.0 INTRODUCTION

In accordance with the U.S. Environmental Protection Agency (EPA) Administrative Order on Consent with Corrective Action Plan (CAP) dated February 27, 1991 (EPA Docket No. VI-001(h)-90-H; EPA I.D. No. TXT490011293), as amended, Formosa Plastics Corporation, Texas (FPC-TX) has undertaken measures to characterize and remediate soil and groundwater affected by volatile organic compounds (VOCs) at the Point Comfort facility. The FPC-TX facility is located in Calhoun County along State Highway 35 and Farm to Market Road (FM) 1593, adjacent to Lavaca Bay (Figure 1). The EPA's 1991 Order addresses a facility of approximately 256 acres.

The overall objective for groundwater cleanup is described in the Final Remedy Decision document of March 11, 2010, which includes specific Corrective Action Objectives (CAOs) for the final remedy to attain. The first CAO describes the groundwater plume containment goal:

Corrective Action Objective 1: The groundwater cleanup objective is to contain the plume, rather than return the groundwater to its maximum beneficial use throughout the plume. The groundwater point of compliance (POC) for FPC will be at the Facility boundary (including the former Brookings property), where concentrations of chemicals of concern must be less than or equal to the maximum contaminant limits (MCLs) for drinking water. (In the event an MCL is not established for a chemical of concern, a risk-based action level will be developed.)

As documented in the Final Risk Management Plan (RMP) (Tetra Tech, 2010), remaining Solid Waste Management Units (SWMUs) and associated potentially impacted soil and groundwater have been segregated into two distinct Areas of Concern (AOC) at the FPC-TX facility: AOC 1 – the former Waste Water Treatment Plant (WWTP) area located in the eastern portion of the site; and AOC 2 – the Vinyl Chloride Monomer (VCM) Process area located in the central portion of the facility.

In July 2012, FPC-TX submitted a work plan (PBW, 2012a) for conducting a bench-scale treatability study of soil and groundwater from the VCM and former WWTP areas. The work plan was approved by EPA in August 2012. The work plan proposed the evaluation of technologies to support CAO 2 of the Final Remedy Decision document:

**Corrective Action Objective 2:** 

To support the final groundwater cleanup objective, FPC must <u>remove</u> or <u>treat</u> source material in soils and/or groundwater to the extent practicable. Using the Texas Risk Reduction Program (TRRP), soils with concentrations of COCs in excess of the soil saturation limit ( $C_{\text{sat}}$ ) must be addressed, and groundwater with concentrations of COCs in excess of 1% solubility must be addressed through removal or treatment.

Three technologies were evaluated for viability in addressing source material:

- 1) In-situ chemical oxidation (ISCO) treatment;
- 2) In-situ bioremediation treatment;
- 3) Dual-phase extraction and removal removal.

This report provides the results and conclusions of the treatability study performed per the approved work plan.

#### 2.0 BACKGROUND

Soil and groundwater affected by volatile organic compounds (VOCs) are present at Formosa's Point Comfort facility. A comprehensive summary of existing environmental data was provided in the Areas of Concern Characterization Work Plan (Tetra Tech, 2012) and is not reproduced here. The Final Risk Management Plan (RMP) (Tetra Tech, 2010) also includes a detailed discussion of the nature and extent of potential soil and groundwater impacts and a conceptual site model (CSM). Both of the summaries mentioned above describe the results of the RCRA Facility Investigation (RFI) (C-K Associates, Inc., 1995). Further investigation of site soil and groundwater in the VCM and former WWTP areas was performed recently per the AOC Characterization Work Plan (Tetra Tech, 2012), as documented in the AOC Characterization Report (PBW, 2012b).

The main constituent of potential concern (COPC) identified in site soil and groundwater is 1,2-Dichloroethane (EDC). Other chlorinated hydrocarbons are also present in soil and groundwater samples at lower concentrations (e.g., chloroform, 1,1,2-trichloroethane, cis-1,2-dichoroethane, trans-1,2-dichloroethane, trichloroethene, vinyl chloride). There are two main areas at the site with COPCs at elevated concentrations: the former Waste Water Treatment Plant (WWTP) area in the eastern portion of the site and the VCM Process area in the central portion of the site. These areas are shown on Figure 2 as Areas of Concern (AOC) 1 and 2, respectively.

In the RMP, the Texas Risk Reduction Program (TRRP) protective concentration levels (PCLs) were used as a screening tool and compared to existing soil data. The <sup>GW</sup>Soil<sub>Ing</sub> PCL (representing the soil-to-groundwater leaching and potential groundwater ingestion pathway) and the <sup>Tot</sup>Soil<sub>Comb</sub> PCL (representing the inhalation, ingestion and dermal contact soil pathways) were identified as the most appropriate screening values. The <sup>Tot</sup>Soil<sub>Comb</sub> PCL is generally several orders-of-magnitude higher than the <sup>GW</sup>Soil<sub>Ing</sub> PCL for the COPCs at the site. As discussed in the RMP, contaminant concentrations in excess of the <sup>Tot</sup>Soil<sub>Comb</sub> PCL were identified in soil samples collected at six SWMUs. Therefore, these areas represent the primary impacted soil areas at the site:

- SWMU #1 Storm Water Basin;
- SWMU #21/22/23 Inactive units adjacent to the active incineration area;
- SWMU #3 Surge Basin; and
- SWMU #4 Emergency Basin.

Evaluation of the existing soil data for the site also included an analysis of whether the soil samples collected during the RFI were from unsaturated soil or saturated soil. The saturation of the soil is an important factor in the consideration of remedial alternatives for soil since saturated soil is best

remediated via groundwater remediation technologies. The analysis of the soil data indicated that the soil samples from the interior of the Surge Basin and Emergency Basin are representative of unsaturated soil conditions. Coupled with the relatively high concentrations of EDC in the samples from these basins, these locations were considered ideal for collection of soil samples for treatability testing.

In the RMP, groundwater concentration data were evaluated for both elevated concentrations and trends. In the context of this work plan, the trend evaluation is less important than the elevated concentrations, since the treatability tests will be performed on groundwater that currently exhibits elevated COPC concentrations. In the RMP, wells where EDC concentrations in groundwater samples exceed or have exceeded one percent (1%) of the aqueous solubility for EDC (87 mg/L), thus defining the potential source areas, are as follows:

#### AOC 1:

- P-56 Zone A, WWTP
- P-57 Zone A, WWTP
- RS-6 Zone A, WWTP

#### AOC 2:

- P-3 Zone A, VCM
- P-36 Zone A, VCM
- RS-3 Zone A, VCM
- RS-1 Zone A/B, VCM
- P-12 Zone B, VCM
- RD-3 Zone B, VCM
- D-11 Zone C, VCM
- D-41 Zone C, VCM
- RD-1- Zone C, VCM
- D-2 Zone C, VCM

Although EDC concentrations, and occasionally chloroform concentrations exceed 1% of the aqueous solubility limit in some samples, dense non-aqueous phase liquid (DNAPL) has not been observed in monitoring wells at the site. This may potentially be due to the age of the release, and that the contaminants may be sorbed-phase sources that can serve as long-term sources of contamination.

Based on the available information summarized above, the Surge Basin and Emergency Basin in AOC 1 appear to be the best locations for treatability studies since these areas have high COPC concentrations and both basins are in the inactive portion of the facility and easily accessible. It can be assumed, because of the known stratigraphy, that any treatment or removal technology that is successful for Zone

A, would be successful for Zones B and C, as each transport zone (A, B, and C) are made up of silty sands and are relatively shallow in depth (depth to top of Zone C occurs about 70 – 80 feet bgs).

#### 3.0 TREATABILITY STUDY DESIGN

#### 3.1 Introduction

Based on the specific characteristics of the site (e.g., groundwater quality, concentrations of COPCs in soil and groundwater, subsurface conditions, logistical issues, etc.), three remediation technologies were implemented for treatability testing: 1) in-situ chemical oxidation (ISCO), 2) enhanced bioremediation, and 3) multi-phase extraction (MPE). These three technologies have the potential to help meet the CAOs and remediation goals for the site.

Depending on the technology, treatability testing can be performed in the laboratory (i.e., bench-scale testing) or in the field (pilot-scale testing). Typically, bench-scale testing is performed first (if feasible). If the bench-scale test results are positive and indicate that a particular technology may be effective at a given site, pilot-scale testing may be warranted. Bench-scale testing was chosen to initially evaluate the ISCO and enhanced bioremediation technologies. Multi-phase extraction is not typically performed at the bench-scale level and should be performed as a pilot-scale test at the site where the COCs are present in environmental media. Therefore, the multi-phase extraction test was performed as a pilot-scale test at the FPC-TX site. Multi-phase extraction is also referred to as dual-phase extraction (DPE) in this report.

The following sections describe the treatability testing program designed to evaluate the selected remediation technologies.

#### 3.2 In-Situ Chemical Oxidation (ISCO)

In-situ chemical oxidation (ISCO) uses strong oxidants to reduce the concentrations of targeted contaminants to acceptable levels. ISCO is accomplished by injecting or otherwise introducing the oxidants directly into the contaminated medium (soil or groundwater) to destroy chemical contaminants in place. Chlorinated ethanes such as EDC are amenable to destruction by chemical oxidation and ISCO is potentially an effective treatment method for soil and groundwater impacted by EDC at the site.

This technology is mainly applicable for saturated media including soil and groundwater; however, in some cases ISCO can be configured to address unsaturated soil by artificially saturating the vadose zone to permit treatment.

Based on the review of potential available oxidant chemistries and the properties of site COPCs, two oxidants (reagents) were selected for bench-scale testing: (1) modified Fenton's reagent (MFR), and (2) activated sodium persulfate (ASP). The sodium persulfate was evaluated using two activation methods, (1) heat (ASP-HEAT) and (2) alkali (ASP-ALK). A bench-scale test was performed for each oxidant.

Specific goals of the bench-scale study were to:

- Determine destruction of COPCs for each oxidant;
- Determine whether removal by modified Fenton's reagent is due to destruction or volatilization;
- Evaluate the effect of treatment on secondary water quality parameters;
- Measure soil oxidant demand for activated persulfate (each activator); and
- Estimate the longevity of modified Fenton's reagent in the presence of soil.

Groundwater and soil samples for the ISCO bench scale study were collected from the WWTP Surge Basin/Emergency Basin area. An evaluation of historic groundwater data indicated that samples from wells P-56 and P-57 (Figure 4) typically exhibit elevated concentrations of EDC and were considered suitable for the treatability testing<sup>1</sup>. Soil samples were collected using direct-push technology from borings immediately adjacent to wells P-56 and P-57. The soil samples were collected from the Zone A sand interval from approximately 11.9 to 13.6 feet below ground level (see boring log for well TS-1 in Appendix A). Four separate borings were necessary to collect the volume of material needed for the ISCO bench-scale treatability study (as well the material needed for the bench-scale bioremediation study, see Section 4.3). The borings were drilled as near as feasible to one another. All borings were properly plugged and abandoned immediately after the completion of sampling. The soil samples were collected using standard collection and decontamination techniques that minimized cross-contamination, were immediately placed on ice for preservation, and were shipped to ISOTEC using standard chain-of-custody procedures. Groundwater samples were collected from well P-56 using the same methods used during the quarterly groundwater monitoring events.

In-Situ Oxidative Technologies, Inc. (ISOTEC) of Lawrenceville, New Jersey performed the ISCO bench-scale studies on the site soil and groundwater, as described in their study proposal included in the work plan. ISOTEC's study report is included in Appendix B of this report. The results of the study are described in Section 4.1.

<sup>&</sup>lt;sup>1</sup> The concentrations of EDC in the samples from P-56 and P-57 were 1,299.7 mg/L and 667.1 mg/L, respectively, in the first quarter 2012 sampling event.

#### 3.3 Enhanced Bioremediation

Enhanced bioremediation is a general term used to describe a variety of remedial technologies whereby the natural microbes in the environment are supplemented with additional microbes (bioaugmentation), nutrients, oxygen (aerobic bioremediation) and/or reducing agents (anaerobic bioremediation) to enhance the natural destruction of contaminants. Anaerobic bioremediation (also called reductive dechlorination or bio-chemical reduction) is considered a potential remedial technology for the FPC-TX site since chlorinated hydrocarbons such as EDC are amenable to reductive dechlorination and also for the following reasons:

- 1) The presence of high ethene concentrations from samples of groundwater from wells P-56 and P-57 may be indicative of the presence of anaerobic microorganisms that have adapted to site conditions and are potentially capable of degrading EDC;
- 2) The site groundwater exhibits overall reducing conditions (negative ORP values) and near neutral pH which indicates that conditions may be suitable for reductive dechlorination.

As for ISCO, this technology is mainly applicable for saturated media including soil and groundwater; however, in some cases bioremediation can be configured to address unsaturated soil by artificially saturating the vadose zone to permit treatment.

To evaluate the potential for reductive dechlorination to serve as a remedial technology at the site, a bench-scale treatability study was developed that used FMC Environmental Solutions (FMC) EHC® technology. The EHC technology uses a reagent that includes a controlled-release, integrated carbon (as a nutrient source) and zero-valent iron (ZVI) as a reducing agent to stimulate the reductive dechlorination of chlorinated solvents such as EDC.

As for the ISCO bench-scale study, groundwater and soil samples for the bioremediation bench scale study were collected from the WWTP Surge Basin/Emergency Basin area. The samples were collected at the same time as the samples for the ISCO treatability study.

FMC performed the enhanced bioremediation bench-scale studies on the site soil and groundwater, as described in their study proposal included in the work plan. FMC's study report is included in Appendix C of this report. The results of the study are described in Section 4.2.

#### 3.4 Mass Removal Pilot Testing

Dual-phase extraction (DPE) (also called dual-phase recovery) is a proven contaminant mass removal technology for highly-contaminated source areas such as those identified at the site. Dual-phase extraction removes contaminants from both groundwater and vadose soils. Extraction from the vadose zone alone is called soil vapor extraction (SVE). Dual-phase extraction can be successful in a low permeable, low yield, heterogeneous formation such as that at the FPC-TX site and can achieve high contaminant mass removal rates. A dual-phase extraction system at the FPC-TX site could potentially remove a substantial portion of the contaminant mass in a relatively short period of time, thus reducing the overall remediation cost.

Gainco Inc. (Gainco) performed mass removal testing by removing soil vapor and groundwater from the subsurface by means of a vacuum. The test was performed at the well cluster including P-56, P-57 and RS-6. Well RS-6 was not used because the well casing contains a semi-permanent groundwater extraction pump and piping. Because the wells in this well cluster are relatively close together (less than 20 feet from one another), an additional temporary well was installed to evaluate the radius of influence of the vacuum. The well (TS-2) was installed using a geoprobe and was constructed to a depth of 15 feet below ground surface (bgs) with five feet of screen. For the DPE testing, Gainco provided mobile equipment powered by a self-contained power source and the appropriately sized high vacuum extraction equipment (e.g., liquid ring pump) capable of removing vapor and groundwater from the wells. The pilot test was conducted over two days, with the SVE and baseline groundwater extraction data collected the first day and high vacuum DPE data collected the second day.

Gainco's study report is included in Appendix C. The results of the study are described in Section 4.3.

#### 4.0 STUDY RESULTS

#### **4.1 ISCO**

ISOTEC performed the ISCO study on site soil and groundwater samples as described in their report contained in Appendix B. Per the work plan (PBW, 2012a), ISOTEC used site soil and groundwater to set up a series of test reactors to perform the study. Site soil and groundwater samples were first composited (from the separate containers sent to ISOTEC by PBW). A portion of the composited soil and groundwater was submitted to a laboratory for initial chemical characterization (see Table 1 of this report and Table 1 of Appendix B). The remaining composited soil and groundwater were prepared into a slurry by mixing at a soil-to-water ratio of 2:1 by weight<sup>2</sup>. A total of three tests were performed, one for each of the three reagents (MFR, heat-activated sodium persulfate (ASP-HEAT), and alkali-activated sodium persulfate (ASP-ALK)). All three tests were performed with an oxidant and an activating agent, as shown in the following table.

TEST	OXIDANT	ACTIVATING AGENT
Modified Fenton's Reagent (MFR)	Stabilized hydrogen peroxide (H <sub>2</sub> O <sub>2</sub> )	ISOTEC Catalyst Series 4260 (circum-neutral pH organometallic complex (chelated iron)
Activated Sodium Persulfate – Alkali (ASP-ALK)	Sodium persulfate (Na <sub>2</sub> S <sub>2</sub> O <sub>8</sub> )	Sodium hydroxide (NaOH)
Activated Sodium Persulfate – Heat (ASP-HEAT)	Sodium persulfate (Na <sub>2</sub> S <sub>2</sub> O <sub>8</sub> )	Heat (60°C)

For each test, a total of four reactors were set up, with one reactor serving as the "control' and the remaining three serving as "treatment" reactors. The reactors consisted of 250 mL glass jars with screw-top caps fitted with Teflon septa to facilitate reagent injection. Each reactor consisted of the same quantity of soil/groundwater slurry at the start of the tests. Reagents were evaluated at three doses, as shown in the following table.

OXIDANT DOSE	MOR TEST	ASP-ALK TEST	ASP-PRAT TEST
Low Dose	6.6 g/Kg	6 g/Kg	6 g/Kg
Medium Dose	33.3 g/Kg	30 g/Kg	30 g/Kg
High Dose	66 g/Kg	60 g/Kg	60 g/Kg
Test Duration	3 days	10 days	1 day

<sup>&</sup>lt;sup>2</sup> A 2:1 mixture by weight consisted of 100 grams of soil and 50 ml of water. Water has a density of 1 g/mL.

The duration of the tests ranged from 1 day to 10 days, as shown in the table. At the end of the test, the reactors were "quenched" to terminate the reactions to minimize subsequent VOC loss. The contents of each reactor was then separated into solid and aqueous phases and submitted for the chemical analyses described in the work plan. A summary of the post-test chemical analyses is provided on Table 1 of this report.

The results of post-test chemical analyses of the soil and groundwater indicate that all three reagents were effective at treating EDC and other VOCs detected at the site (Table 1). The maximum EDC and total VOC reduction was greater than 99% in both the solid and aqueous phases. Destruction of EDC was also greater at the higher reagent doses, as would be expected. In general, the medium reagent dose for all three reagents resulted in a minimum 86% reduction in EDC/VOC concentrations. The high reagent dose for all three reagents resulted in a minimum 98% reduction in EDC/VOC concentrations. Among the three reagents, MFR resulted in the greatest EDC/VOC concentration reductions at the low dose. ASP-ALK resulted in the greatest EDC/VOC concentration reductions at the high dose (99.9%).

ISOTEC noted that characteristics of the site also influence the ability of the reagents to reduce EDC/VOC concentrations in soil and groundwater. Iron and manganese concentrations in soil and groundwater are important catalysts in the MFR and persulfate reactions that result in EDC/VOC destruction. The total iron, ferrous iron and manganese concentrations in site groundwater are below the minimum concentrations necessary for proper activation of the reagents. Therefore, external catalyst would be required for field application of these reagents. Furthermore, although iron and manganese are found in site soil, they are mostly in the form of oxyhydroxides. The oxyhydroxides will promote some Fenton-like reactions, but they are generally unavailable to act as effective catalysts and can result in oxidant wastage (i.e., the oxidant is used in chemical reactions other than those responsible for EDC/VOC reduction). Finally, the background total organic carbon (TOC) concentrations in site soil and groundwater are expected to exert a moderate to high oxidant demand (oxidant scavenging). In other words, the TOC will compete with the contaminants for oxidant and result in lower VOC reductions than in a system with less available TOC.

The effects of the reagents on the general chemistry of the treated groundwater were also evaluated during the study (see Table 2 of this report), as follows:

1) pH – The pH of site groundwater is typically in the range of 6-7 standard pH units. The pH of the groundwater from well P-56 was 6.55 at the time of sample collection. The pH of the treated water remained in this general range for the MFR and ASP-HEAT tests. A slight rise in pH was observed in the MFR test; a slight decrease was observed in the ASP-HEAT test. The pH of the

groundwater in the ASP-ALK test increased significantly due to addition of the highly-alkaline sodium hydroxide.

ORP – the ORP of site groundwater is variable, ranging from slightly positive to slightly negative. The ORP of the groundwater from well P-56 was measured at -125 at the time of sample collection. The ORP of the treated groundwater remained stable for the MFR test. The ORP of the treated groundwater decreased during the ASP-ALK test. The ORP increased slightly during the ASP-HEAT test. It is important to note that ORP is a sensitive parameter and is difficult to measure, which may explain the variability observed in the test results.

3) TDS – the TDS of site groundwater is variable, ranging from less than 5,000 mg/L to greater than 10,000 mg/L. The TDS of the groundwater from well P-56 was 9,150 mg/L. The TDS of the treated groundwater increased slightly in the MFR test. The TDS of the treated groundwater increased significantly during the persulfate tests due to the addition of the sulfate present in the reagent.

As noted on page 13 of the ISOTEC report, a bench-scale study only evaluates the oxidation "chemistry" of the various oxidants as it relates to site contaminants and certain site characteristics. In other words, it evaluates whether the oxidants can treat the contaminants present at the site. In the current study performed by ISOTEC, the oxidants were successful in reducing EDC and other VOC concentrations using site soil and groundwater.

Bench-scale conditions are very different from in-situ conditions. For instance, although the 2:1 soil-to-groundwater mixture is an industry standard for bench-scale tests, it does not simulate natural conditions. Natural in-situ conditions typically have a soil-to-water ratio of approximately 5.8:1 (assuming 30% porosity). Furthermore, in-situ soil particles are compacted and inhibit the entry of the oxidants into the particle matrix.

In-situ conditions present a unique set of obstacles relative to bench-scale conditions and the implementation of ISCO remediation in the field is much more complex than in the laboratory. Remediation requires the appropriate combination of injection pressures, volumes and flow rates; reagent type and concentration; and injection spacing — all intended to achieve a uniform distribution of reagents in the subsurface. These parameters have to be linked with the site conditions such as grain size, site stratigraphy, depth to water, etc. For most sites, including the FPC-TX site, actual in-place oxidant loading and concentrations will likely be lower than those in the study to address site conditions such as the presence of interbedded low-permeability soils and a shallow water table.

Finally, ISOTEC observed that the reduction in EDC/VOC concentrations in both the solid and aqueous phases was very limited for both the low-dose persulfate applications, but this was not the case for the low-dose MFR application (see pages 13-14 of the ISOTEC report in Appendix B). Given the site characteristics noted in the previous paragraphs, field applications of ISCO will mimic the low-dose applications. Since contaminant mass reduction typically comes from a cumulative effect of multiple

low-dose applications (as opposed to one medium- or high-dose application), it does not appear that multiple low-dose applications of activated persulfate will lead to cumulative contaminant mass reduction. However, multiple low-dose applications of MFR should produce a cumulative contaminant mass reduction. Based on these conclusions, a field pilot study using MFR as the oxidant is recommended by ISOTEC.

#### 4.2 Enhanced Bioremediation

FMC performed a bench-scale treatability study to evaluate the enhanced bioremediation technology as described in Section 3.2 and in their report in Appendix C. FMC used its EHC® technology which uses controlled-release, integrated carbon (as a nutrient source) and zero-valent iron (ZVI) as a reducing agent to stimulate the reductive dechlorination of chlorinated solvents such as EDC.

Site soil and groundwater samples were first composited (from the separate containers sent to FMC by PBW). A portion of the composited soil and groundwater was submitted to a laboratory for initial chemical characterization. The bench-scale test was set up as outlined in FMC's proposal contained in the work plan (PBW, 2012a) and in their study report included in Appendix C. One EHC treatment microcosm and two control microcosms (groundwater and ambient) were prepared. Sacrificial jars (glass jars with Teflon-lined lids) were set up for the control and treatment microcosms. Two sizes of jars were used (250 mL and 1 L) to allow for sampling of additional parameters during the final sampling event. The groundwater control microcosms were filled with the composited groundwater to zero headspace and capped. The ambient control microcosms contained the homogenized soil (75g for the 250 mL jar; 300 g for the 1 L jar) and were filled with site groundwater to zero headspace and capped. The EHC microcosms were filled with the homogenized site soil, 0.5% EHC reagent (1.5 g for the 250 mL jar; 5.7 g for the 1 L jar), and site groundwater to zero headspace and capped. The mass of EHC was added based on the total mass of soil and groundwater in the microcosms. All microcosms were inverted several times to mix.

Time zero samples were collected from the ambient control (soil plus water) microcosm on the first day of the test. Samples were collected from the water control, ambient control and EHC treatment microcosms at week 4 (Day 28) and week 8 (Day 56). Review of the results from the Day 56 sampling event (Table 3) indicated a low rate of VOC destruction<sup>3</sup> by EHC alone, likely due to either 1) the high

<sup>&</sup>lt;sup>3</sup> The rate of VOC destruction in the EHC treatment microcosm was calculated by comparing the concentration from the EHC treatment microcosm sample for a particular sampling event to the ambient control microcosm sample also collected during that sampling event.

concentrations of EDC and other VOCs were toxic to the natural microbes present; or b) the appropriate microbes were not naturally present at the site. Based on these results, a decision was made to bioaugment the EHC treatment microcosm by adding a commercially-available mixed culture of SDC-9 (Dehalococcoides) and TCA-20 (Dehalobacter). Bioaugmentation was conducted on day 85 of the test. A sampling event was conducted in week 14 (Day 99), the results of which again indicated poor destruction of VOCs. Therefore, the low rate of destruction of VOCs is thought to be due to the high concentrations of EDC and VOCs in the soil and groundwater used for the tests, not the absence of the appropriate microbes at the site. The test was terminated after review of the Day 99 results and a final report prepared (Appendix C).

In summary, the EHC treatment with bioaugmentation did not result in significant reductions in EDC concentrations in the samples. At Day 99 of the test, the concentration of EDC in the EHC treatment microcosm was reduced by 33.6% compared to the ambient control microcosm. A similar reduction in total VOCs was observed (35.9%). Although the rate of EDC destruction was low, other VOCs showed better rates of destruction (e.g., chloroform), presumably as a result of reductive dechlorination.

#### 4.3 Mass Removal

Gainco performed the mass removal study at well cluster P-56/P-57/RS-6, as described in their report contained in Appendix D. Per the work plan (PBW, 2012a), Gainco performed a three-phase test to determine whether SVE or high vacuum DPE technology is suitable for remediation of the site. The test apparatus consisted of a liquid ring pump connected to a 1-inch diameter PVC pipe (stinger) that was inserted into well P-57 (the "extraction well" in the context of this test). Stage 1 was performed by applying a vacuum in a step-wise fashion in well P-57 with the stinger approximately 9-10 feet above the water level and with the annular space between the stinger and well casing sealed. The duration of the test was 90 minutes and measurements of vacuum were taken from wells P-57, P-56, and temporary well TS-2 that was installed for the purposes of this study. Stage 2 of the study consisted of a short-term pump test performed with the stinger placed near the bottom of well P-57. Water-level measurements were taken from wells P-56 and TS-2 during the test to allow for estimation of aquifer properties. Stage 3 of the study evaluated DPE by applying a constant vacuum in well P-57 with the stinger below the water level and with the annular space between the stinger and the well casing sealed. Measurements of groundwater extraction rate, subsurface vacuum, volatile organic compound concentration (via a photoionization detector) were collected during the six-hour test.

The results of the study are included in the Gainco report contained in Appendix D, including tables, figures and graphs. The major conclusions of the study are:

- 1) The average mass of hydrocarbons removed was approximately ten times greater with high-vacuum DPE than with SVE alone (0.83 lb/hr for DPE versus 0.072 lb/hr for SVE). Although the low permeability of the soil at the site reduces overall effectiveness, the relatively high volatility of EDC and the other hydrocarbons present at the site make these contaminants viable candidates for remediation via DPE. SVE alone is not likely a suitable remedial technology for the site.
- 2) The hydrocarbon mass removal was low using SVE alone. Attempts to apply a high vacuum in well P-57 using SVE alone resulted in an increase in the water level above the well screen, precluding the removal of soil vapor using this method. These results are likely due to the relatively low permeability of the soils present at the site. As mentioned above, SVE alone is not likely a suitable remedial technology for the site.
- 3) The radius of influence (ROI) of the vacuum in the subsurface predicted by the tests was 7.5 feet for SVE and 11.5 feet for DPE.
- 4) The average groundwater recovery rate during the pump test (Stage 2) was 0.57 gallons per minute (gpm). The average groundwater recovery rate during the DPE test (Stage 3) was 0.49 gpm.
- 5) The hydraulic conductivity of the Zone A sand interval estimated by the pump test (Stage 2) was 1.34 x 10<sup>-2</sup> cm/sec (38 ft/day). This estimate is approximately one order of magnitude greater than previous estimates of the hydraulic conductivity of the Zone A sand at this location and at other locations at the site.

Based on these conclusions, DPE remains a potentially viable remediation alternative for the site. Further evaluation of DPE should be conducted by performing a pilot-scale test of longer duration (e.g., three days).

#### 5.0 CONCLUSIONS

#### **5.1** ISCO

The results of post-test chemical analyses of the soil and groundwater indicate that all three ISCO reagents were effective at treating EDC and other VOCs detected at the site. The maximum EDC and total VOC reduction was greater than 99% in both the solid and aqueous phases. Destruction of EDC was also greater at the higher reagent doses, as would be expected.

Iron and manganese concentrations in soil and groundwater are important catalysts in the FMR and persulfate reactions that result in EDC/VOC destruction. The total iron, ferrous iron and manganese concentrations in site groundwater are below the minimum concentrations necessary for proper activation of the reagents. Therefore, external catalyst would be required for field application of these reagents. Also, the background total organic carbon (TOC) concentrations in site soil and groundwater are expected to exert a moderate to high oxidant demand (oxidant scavenging).

A limitation of the study is that a bench-scale study only evaluates the oxidation "chemistry" of the various oxidants as it relates to site contaminants and certain site characteristics. For the current study performed by ISOTEC, the oxidants were successful in reducing EDC and other VOC concentrations using site soil and groundwater. However, in-situ conditions present a unique set of obstacles relative to bench-scale conditions and the implementation of ISCO remediation in the field is much more complex than in the laboratory. Remediation requires the appropriate combination of injection pressures, volumes and flow rates; reagent type and concentration; and injection spacing – all intended to achieve a uniform distribution of reagents in the subsurface. These parameters have to be linked with the site conditions such as grain size, site stratigraphy, depth to water, etc. For most sites, including the FPC-TX site, actual in-place oxidant loading will likely be lower than in the study to address site conditions such as the presence of interbedded low-permeability soils and a shallow water table.

Finally, ISOTEC observed that the reduction in EDC/VOC concentrations in both the solid and aqueous phases was very limited for both the low-dose persulfate applications, but this was not the case for the low-dose MFR application. Given the site characteristics, field applications of ISCO will mimic the low-dose applications. Since contaminant mass reduction typically comes from a cumulative effect of multiple low-dose applications (as opposed to one medium- or high-dose application), it does not appear that multiple low-dose applications of activated persulfate will lead to cumulative contaminant mass reduction. However, multiple low-dose applications of MFR should produce a cumulative contaminant

mass reduction. Based on these conclusions, a field pilot study using MFR as the oxidant is recommended by ISOTEC.

#### 5.2 Enhanced Bioremediation

The EHC treatment did not result in significant reductions in EDC concentrations in the bench test samples over a period of 99 days. The low rate of EDC destruction is likely due to the high concentrations of EDC and other VOCs present in the samples, which were toxic to the natural microbes present. Furthermore, bioaugmentation of the samples during the bench test with common cultures did not result in significant reductions in EDC concentrations.

#### 5.3 Mass Removal

The three-stage mass removal pilot test evaluated SVE alone and DPE as potential remedial technologies for the site. The study results indicated that SVE alone is not viable at this site due to the relatively low permeability of the soils at the site. In the pilot test, the application of a high vacuum increased the groundwater level in the well, precluding the removal of vapor phase contamination from the vadose zone.

The average mass of hydrocarbons removed was approximately ten times greater with high-vacuum DPE than with SVE alone. Although the low permeability of the soil at the site reduces overall effectiveness, the relatively high volatility of EDC and the other hydrocarbons present at the site make these contaminants viable candidates for remediation via DPE. Further evaluation of DPE should be conducted by performing a pilot-scale test of longer duration (e.g., three days).

#### 6.0 REFERENCES

- C-K, 1995. C-K Associates, Inc. Supplemental RCRA Facility Investigation. Prepared for Formosa Plastics Corporation, Texas. June. Revised May 1998.
- Pastor, Behling & Wheeler, LLC (PBW), 2012a. Bench-Scale Treatability Testing Work Plan. Prepared for Formosa Plastics Corporation, Texas. July.
- Pastor, Behling & Wheeler, LLC (PBW), 2012b. AOC Characterization Report. Prepared for Formosa Plastics Corporation, Texas. November.
- Tetra Tech, 2010. Final Risk Management Plan. Prepared for Formosa Plastics Corporation, Texas. April 30.
- Tetra Tech, 2012. Areas of Concern Characterization Work Plan. Prepared for Formosa Plastics Corporation, Texas. May 4.

TABLE 1. ISCO TESTS DATA SUMMARY - EDC AND VOCs

470,000 185,000 30,600	TOTAL VOCs 1,408,780 ED FENTON'S REAG 519,980 208,760 35,114 10,676	EDC REDUCTION ENT TEST 60.64% 93.49%	 59.85%
MODIFII 470,000 185,000 30,600 8 190	519,980 208,760 35,114	60.64%	 59.85%
MODIFII 470,000 185,000 30,600 8 190	519,980 208,760 35,114	60.64%	 59.85%
185,000 30,600 8 190	208,760 35,114		59.85%
30,600 8 190	35,114		59.85%
30,600 8 190		02 /10%	22.250/
8 190	10.676		93.25%
ALKALI-ACTI\	10,670	98.26%	97.95%
	ATED SODIUM PE	RSULFATE TEST	<u> </u>
652,000	700,690		25.400/
497,000	524,220	23.77%	25.19%
	92,888		86.74%
243	667.86		99.90%
HEAT-ACTIV	ATED SODIUM PER	RSULFATE TEST	T
	806,720	<b></b>	
	612,240	23.86%	24.11%
	38,372	99.63%	95.24%
	16,901	99.97%	97.90%
SOLID PH	ASE (concentratio	ns in mg/Kg)	AN GOOD ASSESSED
EDC	TOTAL VOCs	EDC REDUCTION	VOC REDUCTION
44.9	47.4		
MODIF	IED FENTON'S REA	GENT TEST	1
	67.1		
	17.7	73.95%	73.66%
	0.01	99.98%	99.98%
0.0063	0.01	99.99%	99.99%
AI KALI-ACT	IVATED SODIUM P	ERSULFATE TEST	
	122.52		
	129.01	Increase	Increase
	13.63	88.97%	88.88%
0.063	0.06	99.85%	99.95%
HEAT-ACT		ERSULFATE TEST	
	77.24		
·	78.40	Increase	Increase
1		99.34%	97.19%
1		99.93%	98.69%
	86,100 243 HEAT-ACTIV 746,000 568,000 2,750 200 SOLID PH EDC 44.9 MODIF 64.10 16.7 0.011 0.0063 ALKALI-ACT 116 124 12.8	86,100 92,888 243 667.86  HEAT-ACTIVATED SODIUM PER 746,000 806,720 568,000 612,240 2,750 38,372 200 16,901  SOLID PHASE (concentration EDC TOTAL VOCS 44.9 47.4  MODIFIED FENTON'S REA 64.10 67.1 16.7 17.7 0.011 0.01 0.0063 0.01  ALKALI-ACTIVATED SODIUM PER 116 122.52 124 129.01 12.8 13.63 0.063 0.06  HEAT-ACTIVATED SODIUM PER 74 77.24 75 78.40 0.487 2.17	86,100         92,888         86.79%           243         667.86         99.96%           HEAT-ACTIVATED SODIUM PERSULFATE TEST           746,000         806,720            568,000         612,240         23.86%           2,750         38,372         99.63%           200         16,901         99.97%           SOLID PHASE (concentrations in mg/kg)           EDC         TOTAL VOCs         EDC REDUCTION           44.9         47.4            MODIFIED FENTON'S REAGENT TEST           64.10         67.1            16.7         17.7         73.95%           0.011         0.01         99.98%           0.0063         0.01         99.99%           ALKALI-ACTIVATED SODIUM PERSULFATE TEST         116         122.52            124         129.01         Increase           12.8         13.63         88.97%           0.063         0.06         99.85%           HEAT-ACTIVATED SODIUM PERSULFATE TEST           74         77.24            75         78.40         Increase           0.487         2.17

Notes:

<sup>1)</sup> See ISOTEC report (Appendix B) for complete data and discussion.

TABLE 2. ISCO TESTS DATA SUMMARY – GENERAL PARAMETERS

Same			. De rollent and it	QUEOUS PHA	SE (concentration	rs in ug/L)	Name of the last		8 II - 13 - 14 - 1	Nitrate
The state of the last of the state of the st	pН	ORP	TDS (mg/L)	Fe2+	Sulfate (SO <sub>4</sub> )	TOC				•
	(SU)	(mV)		(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)
NITIAL COND.	6.55	-125	9,150	4,960	378,000	8,540	8,710	7,930	606,000	ND (<500)
NITIAL COND.	0.55			MODIFIED F	ENTON'S REAGE	NT TEST		,	<u></u> .	<del></del>
	6.51	185	5,940	< 40						
Control	6.63	182	6,286	< 40						
Low Dose	6.90	189	8,220	< 40						
Medium Dose	7.15	203	11,070	< 40						
High Dose	7.13	203	AL.	KALI-ACTIVAT	ED SODIUM PERS	ULFATE TEST				
<del></del>	6.6	46	10,880							
Control		-159	18,340						<del></del>	
Low Dose	11.36	-199	48,500		4-					
Medium Dose	12.06	-211	91,740						,	
High Dose	12.25	-211	) J.,,,,,,	FAT-ACTIVATE	D SODIUM PERS	JLFATE TEST			<b>.</b>	<del></del>
		34	11,170			T				
Control	6.57	48	19,040							
Low Dose	6.18			No.						
Medium Dose	6.02	57	36,150	<del></del>		<del> </del>			:	
High Dose	5.37	99	55,300			in ma/Ka)				- 8
e programa de la composició de la compos	والمرافع وسوو	ne ne ender	orania de la compositione de la compositione de la composition de la compositione de la c	SOUD PHASE	E (CONCENTRALIONS	TOC	Total Iron	Manganese		
						(mg/Kg)	(mg/Kg)	(mg/Kg)		
						1,190	5,640	136		
INITIAL COND.			m-	<u></u>		1,130	1 3,040		<u></u>	

Notes:

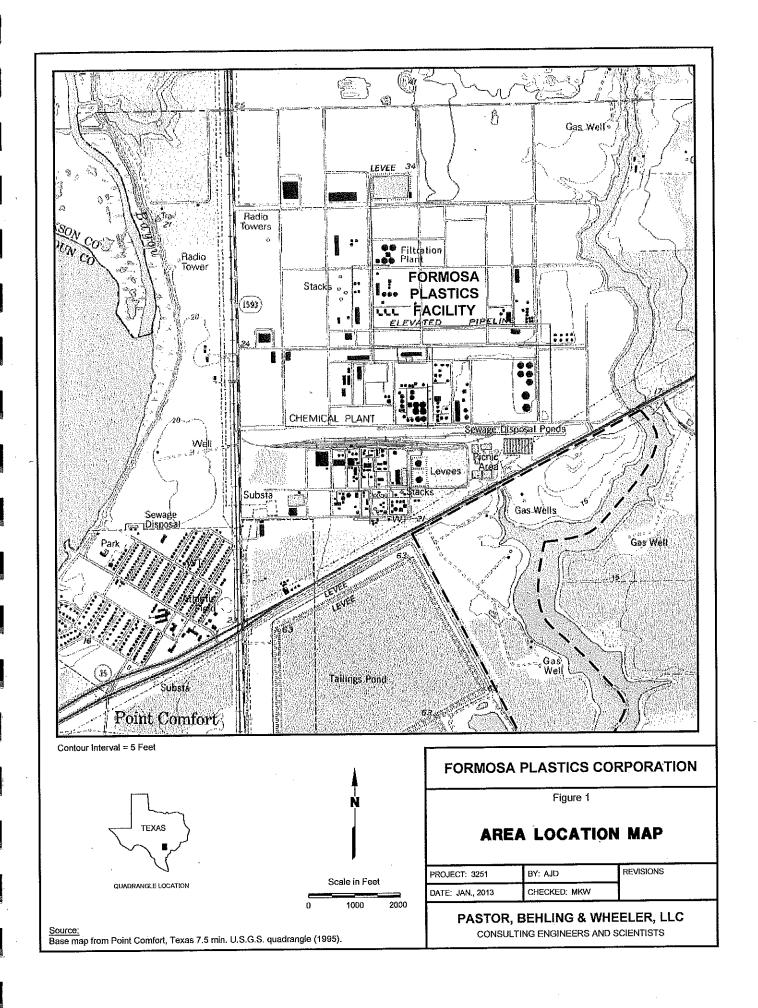
<sup>1)</sup> See ISOTEC report (Appendix B) for complete data and discussion.

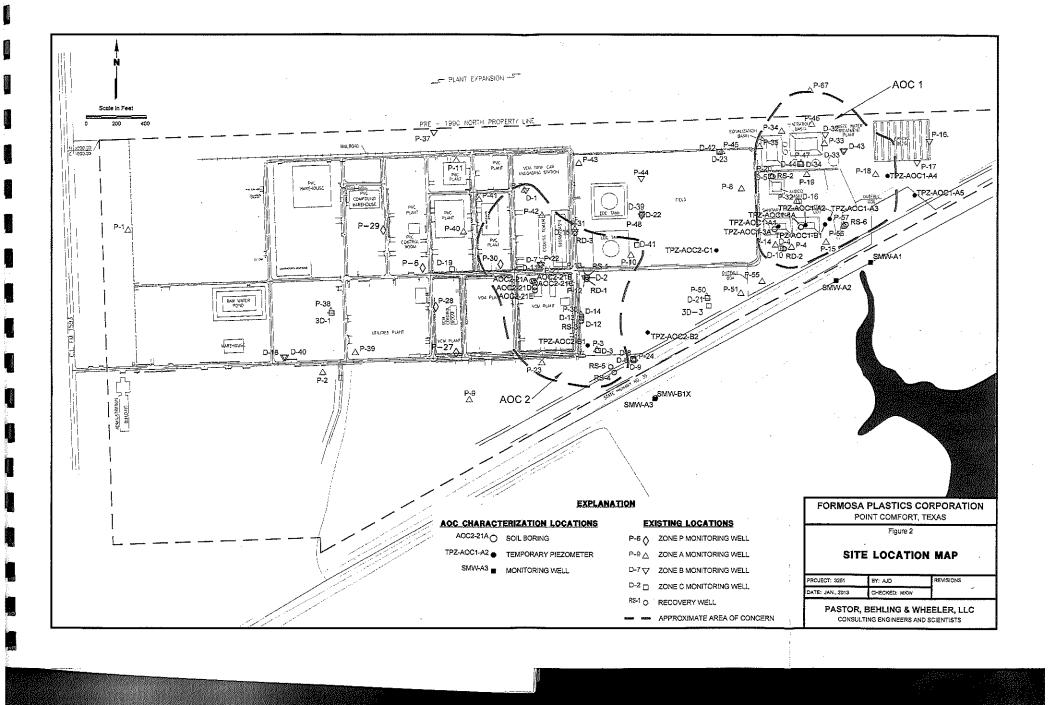
TABLE 3. ENHANCED BIOREMEDIATION TEST DATA SUMMARY - EDC AND VOCs

TEST RESULTS (concentrations in ug/L)					
15 Ayrilla (1972) 1973   1975	EDC	TOTAL VOCs	EDC REDUCTION	VOC REDUCTION	
	INITIAL CONDITIONS				
Groundwater	1,400,000	1,554,800			
Soil	38,000	40,312			
	WATE	R CONTROL MICRO	COSMS		
Time Zero (Ambient)	1,500,000	1,623,600			
Day 28	1,200,000	1,335,500	20% (2)	17.7%	
Day 56	1,400,000	1,530,000	6.7%	5.8%	
Day 99	1,100,000	1,168,200	26.7%	28%	
	AMBIE	NT CONTROL MICRO	OCOSMS	•	
Time Zero (Ambient)	1,500,000	1,623,600	<b></b>	**-	
Day 28	1,100,000	1,243,100	26.7% <sup>(2)</sup>	23.5%	
Day 56	1,300,000	1,419,400	13.3%	12.6%	
Day 99	1,400,000	1,520,000	6.7%	6.4%	
Day 33	EHC 1	REATMENT MICRO	COSMS		
Time Zero (Ambient)	1,500,000	1,623,600			
Day 28	990,000	1,090,300	10% (3)	12.3%	
Day 56	1,100,000	1,162,030	15.4%	18.1%	
Day 99 <sup>(4)</sup>	930,000	974,800	33.6%	35.9%	

#### Notes:

- 1) See FMC report (Appendix C) for complete data and discussion.
- 2) Percent reduction in the water and ambient control microcosms was calculated by dividing the concentration into the time zero ambient control concentration.
- 3) Percent reduction in the EHC treatment microcosm was calculated by dividing the concentration into the corresponding ambient control microcosm concentration.
- 4) After bioaugmentation of the EHC microcosm.





APPENDIX A

Boring Log for TS-1

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Sonic
579
38
M. You had I a may
of section, moist,
<u>-</u>
•

APPENDIX B

ISOTEC Report - ISCO



# BENCH SCALE TREATABILITY STUDY REPORT

FORMOSA PLASTICS CORPORATION POINT COMFORT, TEXAS

**JANUARY 11, 2013** 

PREPARED FOR

PASTOR, BEHLING & WHEELER, LLC 620 E. AIRLINE ROAD VICTORIA, TEXAS 77901

**ISOTEC PROJECT No. 901132** 

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ATTACHMENT A..... BENCH STUDY ANALYTICAL DATA PACKAGES

## **ACRONYMS**

ASP Activated sodium persulfate
ASP-alk Alkali activated sodium persulfate
ASP-heat Heat activated sodium persulfate

COCs Constituents of concern

expt Experiment

g gram
g/kg Grams per kilogram
Groundwater

GW Groundwater

IAL Integrated Analytical Laboratories, LLC

ISCO In-situ chemical oxidation

In-Situ Oxidative Technologies, Inc.

Lbs Pounds

MFR Modified Fenton's Reagent mg/kg Milligrams per kilogram

mg milligram
ml milliliter
mV milli volt

NaOH Sodium hydroxide Na<sub>2</sub>S<sub>2</sub>O<sub>8</sub> Sodium persulfate

ND Non detect concentration
PBW Pasto, Behling & Wheeler, LLC

ppm Parts per million
TDS Total dissolved solids
TOC Total organic carbon
TOD Total oxidant demand
ug/kg Micrograms per kilogram
µg/L Micrograms per liter

VOC Volatile organic compound

#### 1.0 EXECUTIVE SUMMARY

In-Situ Oxidative Technologies, Inc. (ISOTEC<sup>SM</sup>) was retained by Pastor, Behling & Wheeler, LLC (PBW) to conduct an in-situ chemical oxidation (ISCO) bench-scale laboratory treatability study (study) on soil and groundwater (GW) samples collected from the Formosa Plastics Corporation (Formosa) site located in Point Comfort, Texas. The target constituents for the study are volatile organic compounds (VOCs), and the constituent of concern (COC) at the site is 1,2-dichloroethane (EDC). Reagents evaluated during the study were modified Fenton's reagent (MFR) and sodium persulfate activated with alkali (ASP-alk) and heat (ASP-heat). The objective of the bench scale study was to evaluate the potential effectiveness of MFR, ASP-alk and ASP-heat in the treatment of EDC impacted soil and groundwater at the site. In addition, total oxidant demand (TOD) for ASP (measured as sodium persulfate) were also evaluated. TOD for MFR was not performed as consumption of hydrogen peroxide (by the activating agent in the MFR reagent to generate hydroxyl free radicals) is nearly 100% in most cases.

PBW collected soil and GW samples from the site and shipped them to ISOTEC for use during the treatability study. Prior to initiating the study, soil and groundwater were first composited, and a portion of the composited soil and composited GW was then collected and submitted to Integrated Analytical Laboratories, LLC (IAL) for various chemical analyses to collect initial characteristics data of the samples.

The remaining composited soils and GW were prepared into a slurry form by mixing the composited soil with the GW at a soil-to-water ratio of 2:1 by weight. All experiments were performed on the 2:1 slurry samples. A total of three experiments were performed, one for each reagent. For each test, a total of four reactors were set up with one reactor serving as the "control" and the remaining three served as "treatment" reactors. Each reactor consisted of the exact same quantity of composited soil and groundwater prior to the start of the experiments. Reagents were evaluated at three doses as shown in the table below. The experiments were quenched upon the completion of the tests. All reactors were separated into aqueous and solid phases and submitted for various chemical analyses on each phase.

#### **Experiment Summary**

Oxidant dose	MFR-test	ASP-alk-test	ASP-heat-test
Low dose	6.6 g/kg	6 g/kg	6 g/kg
Medium dose	33.3 g/kg	30 g/kg	30 g/kg
High dose	66 g/kg	60 g/kg	60 g/kg
Test Duration	3 days	10 days	1 day

Note: Oxidant doses are presented as grams of oxidant per kilogram of soil being tested.

Results indicate that all three reagents were effective in treating EDC as well as other VOCs detected at the site. Summary results are presented below.

- Using MFR, EDC was treated from 470,000 micrograms per liter (μg/L) to 185,000 μg/L following the low dose treatment, and further down to 30,600 μg/L (medium dose) and 8,190 μg/L (high dose) in the aqueous phase, and from 64.1 milligrams per kilogram (mg/kg) to 16.7 mg/kg (low dose) and 0.0063 mg/kg (high dose) in the solid phase. VOC reductions achieved were 60% (low dose), 93% (medium dose) and 98% (high dose) in the aqueous phase and 74% (low dose) and >99% (medium and high doses) in the solid phase.
- Using ASP-alk, EDC was treated from 652,000 μg/L to 497,000 μg/L (low dose), 86,100 μg/L (medium dose) and 243 μg/L (high dose) in the aqueous phase. In the solid phase, EDC was treated from 116 mg/kg to 12.8 mg/kg (medium dose) following a slight increase with the low dose application and further down to 0.06 mg/kg (high dose). VOC reductions achieved were 25% (low dose), 87% (medium dose) and >99% (high dose) in the aqueous phase and 89% (medium dose) and >99% (high doses) in the solid phase. TOD analyses indicated 26%-57% consumption of sodium persulfate (Na<sub>2</sub>S<sub>2</sub>O<sub>8</sub>) applied during the 10 day test period with an oxidant demand of 3.42 g/kg for the low dose, 9 g/kg for the medium dose and 15.6 g/kg for the high dose.
- Using ASP-heat, a similar EDC/VOC reduction pattern to that of ASP-alk was observed. EDC was treated from 746,000 μg/L to 568,000 μg/L (low dose), 2,750 μg/L (medium dose) and 200 μg/L (high dose) in the aqueous phase. In the solid phase, EDC was treated from 74 mg/kg to 0.487 mg/kg (medium dose) following a slight increase with the low dose application and further down to 0.05 mg/kg (high doses). VOC reduction achieved were 25% (low dose), 95% (medium dose) and 98% (high dose) in the aqueous phase and 97% (medium dose) and 99% (high doses) in the solid phase. TOD analyses indicated 53%-72% consumption of Na<sub>2</sub>S<sub>2</sub>O<sub>8</sub> applied during the 1 day test period with an oxidant demand of 4.32 g/kg for the low dose, 18.9 g/kg for the medium dose and 31.8 g/kg for the high dose.
- One observation of the bench study data is unique and important. The reduction in concentration in both solid and aqueous phases was very limited in both low-dose persulfate applications, while the MFR low-dose application showed a 61% and 74% VOC reduction for aqueous and solid phase, respectively. Total contaminant mass reduction comes from a cumulative effect of multiple low-dose applications, as opposed to one large medium-dose application; due primarily to field injection limitations of reagent volume and concentration. It does not appear that multiple low-dose applications of activated persulfate will lead to a cumulative mass reduction, since individual low-dose applications are

Bench Scale Treatability Study Report Formosa Plastics Facility, Point Comfort, Texas ISOTEC Project #901132

relatively ineffective. However, multiple low-dose applications of MFR should produce a cumulative mass reduction.

#### 2.0 BENCH SCALE STUDY OBJECTIVES

The objectives of the bench scale study are to:

- > Evaluate the treatment effectiveness of MFR, ASP-alk and ASP-heat in the treatment of VOCs, primarily EDC.
- > Determine the total oxidant demand (TOD) for ASP-alk and ASP-heat.

### 3.0 SAMPLE COLLECTION AND PREPARATION

PBW collected soil (TS-1) and GW (P-56) samples on Sept. 5, 2012 from the site and shipped them to the ISOTEC research facility for use during the treatability study. The samples were stored at  $<4^{\circ}$ C during the shipment and at ISOTEC's facility until commencement of each test.

Prior to initiating the study, the soil and groundwater samples were composited. A portion of the composited soils and groundwater was collected for initial characterization. This included analyses of VOCs, total organic carbon (TOC), total iron and total manganese on soil and GW samples, and alkalinity, ferrous iron, nitrate, sulfate and total dissolved solids on the GW sample only.

The experiment samples were prepared by mixing the composited soil with the groundwater at a 2:1 soil to groundwater ratio by weight. The 2:1 ratio was selected to represent a soil matrix that resembles the saturated subsurface with groundwater pore volume representative of 33% porosity. The experiment samples were used to perform various experiments to evaluate the effectiveness of MFR, ASP-alk and ASP-heat.

All samples were submitted to IAL for analyses. TOD analysis was performed internally at the ISOTEC laboratory along with pH, oxidation-reduction potential (ORP) and total dissolved solids (TDS) measurements.

#### 4.0 EXPERIMENTAL PROCEDURES

The bench-scale treatability study consisted of MFR-test, ASP-alk-test and ASP-heat-test. In general, each test comprised of the following 4 steps:

- 1. Reagent Identification,
- 2. Establishing experimental control,
- 3. Experimental setup, and
- 4. Sample analysis.

#### 4.1 Reagent Identification

In accordance to the Treatability Study Proposal, MFR and ASP were to be evaluated in the study. Both MFR and ASP consisted of an oxidant and an activating agent. For MFR, the oxidant used is stabilized hydrogen peroxide ( $H_2O_2$ ) and the activating agent used is ISOTEC's patented Catalyst Series 4260 (Cat-4260), which is a circum-neutral pH (e.g. 5-8) organometallic complex (chelated iron) with high mobility within the subsurface. For ASP, the oxidant used is sodium persulfate ( $Na_2S_2O_8$ ) and the activating agent used is sodium hydroxide (NaOH) for ASP-alk, and heat ( $60^{\circ}$ C) for ASP-heat.

#### 4.2 Establishing Experimental Controls

An experimental "control" sample was set up during each experiment to document the following:

- Reduction or changes in concentrations of the target constituents due to sample dilution by reagent volumes injected.
- Reduction in concentrations of the target constituents due to volatilization caused by room temperature test conditions for MFR and ASP-alk, and the heated conditions for ASP-heat.

The "control" sample was set up exactly the same way, remained at, and was subject to the same conditions as the associated "treatment" reactors. However, the "control" reactor received distilled water (DI) instead of reagent (see Section 4.4 below).

#### 4.3 Experimental Setup

Each experiment was set up in four reactors, one served as the "control" reactor (see Section 4.2 above) and the remaining three reactors as "treatment" reactors to receive MFR and ASP reagents at three dosages (low, medium and high) by weight of soil in the slurry being tested.

The experiments were performed in 250 milliliter (ml) VOC-tight glass jars sealed with screw top caps fitted with Teflon septa to facilitate reagent injection and prevent contaminant volatilization during the experiments. Exactly 150 grams (g) of 2:1 slurry

(100 g of soil and 50 ml of groundwater) was introduced into each reactor. The reactors were set up in duplicates, with one set used for VOC analysis and the second set used for pH, ORP, TDS measurements and TOD monitoring of  $Na_2S_2O_8$  concentrations.

#### 4.4 Reagent Applications

#### 4.4.1 MFR-test

For reagent application, a predetermined amount of MFR was injected into each "treatment" reactor as incremental doses and DI water was used to compensate the differences in reagent volumes applied between reactors. The final oxidant  $(H_2O_2)$  concentrations were 6.6 g/kg (low), 33.3 g/kg (medium) and 66 g/kg (high) by weight of soil in the slurry sample being tested.

The multiple dosage approach (incremental approach) was used to increase treatment efficiency, minimize gas formation (preventing volatilization) and the resulting pressure buildup. For this study, two, four and six injections were performed to achieve the final oxidant concentrations in low dose, medium dose and high dose reactors, respectively. A time gap of approximately eight hours was maintained between dosages. All reactors (control and treatment) were left under room temperature conditions and inverted exactly 10 times daily to gain maximum contact between the reagent and the sample matrix. The duration of the experiment was three days.

#### 4.4.2 ASP-alk-test

The predetermined amount of  $Na_2S_2O_8$  was applied into each "treatment" reactor in a single batch and DI water was used to compensate the difference in reagent volumes applied between reactors. The final oxidant ( $Na_2S_2O_8$ ) concentrations were 6 g/kg (low dose), 30 g/kg (medium dose) and 60 g/kg (high dose) by weight of soil in the slurry sample being tested. The "control" reactor in each experiment received an equivalent volume of distilled water instead of reagent. Alkali activation was achieved by raising and maintaining the pH value of the sample contents in each "treatment" reactor to between 11 and 12 standard unit (su) via addition of NaOH. All reactors (control and treatment) were left under room temperature conditions and inverted exactly 10 times daily to gain maximum contact between the reagent and the sample matrix. The duration of the experiment was 10 days.

#### 4.4.3 ASP-heat-test

Similar to the ASP-alk-test, the predetermined amount of  $Na_2S_2O_8$  was applied into each "treatment" reactor in a single batch and DI water was used to compensate the difference of reagent volumes applied between reactors. The final oxidant  $(Na_2S_2O_8)$  concentrations were 6 g/kg (low dose), 30 g/kg (medium dose) and 60 g/kg (high dose) by weight of soil in the slurry sample being tested. The "control" reactor received an equivalent volume of distilled water instead of reagent. Heat activation was achieved

by placing all reactors (control and treatment) of both sets in a water bath with warm water to raise and maintain the temperature of the sample contents at  $60^{\circ}$ C. The duration of the experiment was one day to minimize the VOC loss under a raised temperature.

For all three tests, a quenching agent (i.e. bovine catalase for peroxide and sodium thiosulfate for sodium persulfate) was injected into each reactor to terminate the reaction at the end of the experiments. Reactors were quenched (even if all the oxidant was not consumed) to minimize COC loss associated with volatilization under room temperature or heated test conditions.

TOD analysis was performed in the corresponding duplicates internally at ISOTEC. The TOD was determined by measuring the initial oxidant measurements (i.e. time = 0 days) collected immediately after introducing the oxidant into each reactor to obtain a baseline starting oxidant concentration. The residual oxidant concentration was obtained at the specific quenching period. TOD is determined from the difference of initial oxidant concentration and the final oxidant concentration. For ASP, TOD was reported as "g/kg" of sodium persulfate. Sodium persulfate concentrations were measured using a CHEMetrics colorimetric testing kit. Final pH, ORP and TDS values were measured using a Myron test kit in the corresponding duplicates.

#### 4.5 Analytical Sample Collection and Analyses

Upon experiment completion, sample contents in each reactor (control and treatment) were separated into aqueous and solid phases. Then analytical samples were collected from each phase and submitted for various analyses as indicated in the table below.

#### **Laboratory Analytical Parameters Summary**

Parameters	Initial Cha	racteristics	MFR-	test	ASP-al	k-test	ASP-he	at-test
	GW	Soil	Aqueous phase	Solid phase	Aqueous phase	Solid phase	Aqueous phase	Solid phase
VOCs	х	х	x	х	х	х	х	х
Ferrous iron	x		х					
Total iron	x	х						
Total manganese	х	х						
Alkalinity	х							
TOC	x	х						
TDS	х							
Sulfate	х							
Nitrate	х							

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IAL performed all chemical analyses associated with the bench-scale treatability study. The VOC analyses was performed using Method SW-846 624 (GW)/8260B (soil), TOC analysis was performed using EPA method modified Lloyd Kahn (soil)/5310C (GW), and total iron and manganese analysis was performed using EPA method 6020, ferrous iron using SM20 3500FeB, alkalinity using 2320B, nitrate using 4500NO3F and TDS using 2540C. Laboratory analytical data packages including chains of custody, and internal laboratory custody chronicle are included as Attachment A.

#### 5.0 RESULTS AND DISCUSSION

Detailed bench-scale testing results (including the initial characteristics analyses and experiment results) are presented in Tables 1 through 4. Laboratory analytical data packages are provided in Attachment A. Initial characteristics results are discussed in Section 5.1 and experiment results are discussed in Sections 5.2.

#### 5.1 Initial Characteristics

Initial characteristics results are presented in Table 1.

In the GW sample (P-56), EDC, the primary site COC, was detected at 1,280,000  $\mu$ g/L. Another 10 VOCs including chloroform (81,600  $\mu$ g/L), vinyl chloride (13,300  $\mu$ g/L) and 1,1-DCA (8,400  $\mu$ g/L) were also detected in the sample resulting in a cumulative VOC concentration at 1,408,780  $\mu$ g/L. Total iron and manganese were detected at 8,710  $\mu$ g/L and 7,930  $\mu$ g/L, respectively, and ferrous iron was found at 4,960  $\mu$ g/L. Based on ISOTEC's past experience, iron concentrations in the aqueous phase should be greater than 25,000  $\mu$ g/L (typical range should be 25,000 to 100,000  $\mu$ g/L) to serve as effective Fenton's catalyst and greater than 150,000  $\mu$ g/L to serve as effective sodium persulfate catalyst. Manganese concentrations greater than 25,000  $\mu$ g/L also have potential to promote Fenton-like reactions. TOC was detected at 8,540  $\mu$ g/L. Alkalinity and sulfate were detected at 606,000  $\mu$ g/L and 378,000  $\mu$ g/L, respectively. Nitrate was found at a non-detectable (ND) level (<500  $\mu$ g/L).

In the soil sample (Soil Comp), EDC was detected at 44.9 mg/kg. Other VOCs detected were chloroform at 2.1 mg/kg and tetrachloroethene (PCE) at 0.4 mg/kg resulting in a total VOC concentration of 47.4 mg/kg. Total iron and manganese were found to be 5,640 mg/kg and 136 mg/kg, respectively. Iron and manganese are present in soils as mostly oxyhydroxides and may promote some Fenton-like reactions, although they are generally unavailable to act as effective catalysts and can potentially result in oxidant wastage. Alkalinity, nitrate, ferrous iron, sulfate and TDS were not analyzed. TOC was detected at 1,190 mg/kg.

TOC in both soil and groundwater will consume oxidants and higher TOC means greater competition for the oxidants, which can result in significant oxidant scavenging. The TOC levels detected in site soils (1,190 mg/kg) and GW (8,540  $\mu$ g/L) are expected to exert a moderate to high oxidant demand. Iron in its dissolved form, especially ferrous iron, present in groundwater is known to activate sodium persulfate and hydrogen peroxide. As noted previously, iron levels in the groundwater (i.e. 8,710  $\mu$ g/L for total dissolved iron and 4,960  $\mu$ g/L for ferrous iron) are lower than the minimum iron concentration requirement for proper activation of sodium persulfate and hydrogen peroxide. Therefore, external catalyst will be needed during field application of MFR and ASP.

#### 5.2 Experiment Results

COC treatment effectiveness is evaluated by comparison of "treated" sample data with the associated "control" sample data. A comparison between the "initial" and "control" data was not made because the analyses were performed on different types of samples (i.e. the "initial" were soil or GW samples, and "control" samples were slurry samples separated into solid and aqueous phases for analyses). However, since the "initial" and "control" samples were both untreated samples, they generally contain similar levels of contamination when sample materials are uniform. The "initial" samples typically have a higher COC concentration compared to "control" since the "control" samples are diluted after addition of DI water and are also subject to the room or heated temperature test conditions similar to the "treated" samples (Section 4.4). [It should be noted that all three "control" samples contained higher VOC levels in the solid phase than the initial soil sample (i.e. Soil Comp). This anomaly is most likely due to heterogeneous nature of the soil samples, which made it almost impossible to produce uniform samples for all the tests and could cause fluctuations in analytical results. The control samples were also mixed with site water containing high VOC concentrations and submitted to the experiment conditions.] As discussed in Section 4.2, a "control" sample was set up for each test to document COC concentration changes due to addition of reagents and VOC loss under the room temperature or heated test conditions. The "control" samples were prepared in the same manner and underwent the same conditions as the corresponding "treated" samples but received zero dosage of reagent. Therefore, the differences in contaminant concentrations between "treated" samples and the associated "control" sample best represent the treatment effectiveness and the effectiveness of each reagent is evaluated by comparison of "treated" sample data with the associated "control" sample data.

For discussion purpose, all ND values are assumed to be equal to zero in the contaminant reduction calculation. As discussed previously, three reagent doses of MFR (6.6 g/kg, 33.3 g/kg, & 66 g/kg of hydrogen peroxide, respectively, for low, medium and high doses) and three reagent doses of ASP (6 g/kg, 30 g/kg, & 60 g/kg of sodium persulfate, respectively, for low, medium and high doses) were evaluated. Results are presented in Tables 2, 3 and 4 and discussed below for each area.

Results indicate that all three reagents were effective in treating VOCs including EDC with maximum reduction achieved by greater than 97% in the aqueous phase and greater than 99% in the solid phase. Detailed discussions are provided below for each test.

#### 5.2.1 MFR-test (Table 2)

A decreasing trend in VOC concentrations is evident as reagent doses increased in both solid and aqueous phases. In the solid phase, EDC was reduced from 64.1 mg/kg to 16.7 mg/kg (74% reduction) following the low dose application. It was further reduced to

0.01 mg/kg (medium dose) and 0.006 mg/kg (high dose), an equivalent 99.9% reduction for both doses. In the aqueous phase, EDC concentrations decreased from 470,000  $\mu$ g/L to 185,000  $\mu$ g/L (low dose), 30,600  $\mu$ g/L (medium dose) and 8,190  $\mu$ g/L (high dose), an equivalent 60%, 93% and 98% reduction.

Similar to EDC, VOC reductions achieved were 73.7% (low dose) and 99.9% (medium and high doses) in the solid phase, and 59.9% (low dose), 93.3% (medium dose) and 98.0% (high dose) in the aqueous phase.

TOD was not evaluated for MFR. In the MFR process, hydrogen peroxide consumption is mainly associated with generation of hydroxyl free radicals (the main agent to attack the organic compounds) through ISOTEC catalyst (the activating agent). The activation of hydrogen peroxide by ISOTEC catalyst is very quick (within hours) and, in most cases very efficient resulting in a nearly 100% consumption of hydrogen peroxide, regardless of the amount of soil or contaminants present.

Final pH ranged between 6.63 and 7.15 with a control value of 6.51. ORP values were between 182 mV and 203 mV with a control value of 185 mV, and TDS ranged between 11  $\mu$ g/L and 8,220  $\mu$ g/L with a control value of 5,940  $\mu$ g/L. Ferrous iron was found at ND (<40  $\mu$ g/L) in all treatment reactors as well as the control reactor.

#### 5.2.2 ASP-alk-test (Table 3)

In the solid phase, EDC slightly increased from 116 mg/kg to 124 mg/kg following the low dose application. This anomaly is most likely due to the heterogeneous nature of the soil as discussed above in Section 5.2. EDC reduction took place following both medium and high doses. EDC concentrations decreased from 116 mg/kg to 12.8 mg/kg and 0.06 mg/kg (high dose), an equivalent 89.0% and 99.9% reduction, respectively. In the aqueous phase, EDC reduced from 652,000  $\mu$ g/L to 497,000  $\mu$ g/L (low dose), 86,100  $\mu$ g/L (medium dose) and 243  $\mu$ g/L (high), an equivalent 23.8%, 86.8% and 99.9% reduction.

For total VOCs, reduction achieved in the solid phase was 88.9% following the medium dose application and 99.9% following high doses. In the aqueous phase, VOC reductions were 25.2% following the low dose, 86.7% following the medium dose application and 99.9% the high dose. The high dose achieved greater than 99% reduction of EDC and total VOCs in both solid and aqueous phases.

TOD measurements showed a  $Na_2S_2O_8$  consumption of 3.42 g/kg for the low dose, 9 g/kg for the medium dose and 15.6 g/kg for the high dose over the 10-day period.

Final pH ranged between 11.36 and 12.25 with a control value of 6.6. ORP values were between -159 mV and -211 mV with a control value of 46 mV. TDS values were noted between 18.34  $\mu$ g/L and 91.74  $\mu$ g/L with a control value of 10.88  $\mu$ g/L.

#### 5.2.3 ASP-heat-test (Table 4)

Using heat activation, a similar EDC/VOC reduction pattern to that of alkali activation was observed. In the solid phase, EDC was slightly increased from 74 mg/kg to 75 mg/kg following the low dose application, most likely due to the heterogeneous nature of the soil. EDC then decreased from 74 mg/kg to 0.487 mg/kg (medium dose) and 0.053 mg/kg (high dose), an equivalent of 99.3% (medium dose) and 99.9% (high dose) reduction. In the aqueous phase, EDC concentrations decreased from 746,000  $\mu$ g/L to 568,000  $\mu$ g/L (low dose), 2,750  $\mu$ g/L (medium dose) and 200  $\mu$ g/L (high), an equivalent 23.9%, 99.6% and 99.9% reduction.

Total VOC reductions achieved were 97.2% (medium dose) and 98.7% (high dose) in the solid phase and 24.1% (low dose), 95.2% (medium dose) and 97.9% (high dose) in the aqueous phase. Therefore, both medium and high doses achieved 98% and greater EDC/VOC reduction.

TOD measurements indicated a 1-day  $Na_2S_2O_8$  consumption of 4.32 g/kg for the low dose, 18.9 g/kg for the medium dose and 31.8 g/kg for the high dose.

Final pH ranged between 5.37 and 6.18 with a control value of 6.57. ORP values were between 48 mV and 99 mV with a control value of 34 mV, and TDS ranged between 19  $\mu$ g/L and 55.3  $\mu$ g/L with a control value of 11.1  $\mu$ g/L.

#### 5.2.4 Results and Discussion

In summary, all three reagents, MFR, ASP-alk and ASP-heat, were effective in treating EDC, the primary site COC, as well as other contaminants detected at the site. In general, using the medium dose, all three reagents were able to achieve 86% and greater EDC/VOC reduction, and using the high dose all three reagents produced approximately 98% EDC/VOC reduction. Among the three reagents, MFR achieved a higher EDC/VOC reduction compared to ASP-alk and ASP-heat at the low dose (60%-73% vs 23%), while ASP-alk produced best results at the high dose leaving the lowest residual VOC concentration in the aqueous phase (667  $\mu$ g/L) compared to MFR (10,676  $\mu$ g/L) and ASP-heat (16,900  $\mu$ g/L).

#### 6.0 CONCLUSIONS AND RECOMMENDATIONS

Results of the bench scale treatability study indicate that MFR, ASP-alk and ASP-heat are all effective towards treating EDC, the primary site COC by achieving greater than 98% EDC reduction in both aqueous and solid phases. The TOD measurements indicated an oxidant demand of  $Na_2S_2O_8$  was 4.32 g/kg to 31.8 g/kg for ASP-heat, and 3.42 g/kg to 15.6 g/kg for ASP-alk.

#### Chemistry vs. Remediation

A bench scale treatability study can really only evaluate the oxidation "chemistry" of the various oxidants. The Formosa study evaluated the chemistry of MFR, ASP-alk and ASP-heat on the contaminants present in the site soil and groundwater, primarily EDC. In other words, can each oxidant treat the contaminants present? The answer is yes, each oxidant tested can reduce contaminant concentrations in soil and water under bench conditions.

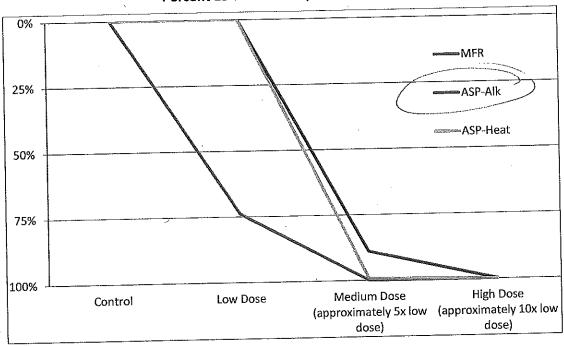
Bench conditions and in-situ conditions are completely different. The bench study started with a soil/water mixture of 2:1 by weight and the soil is comprised of individual particles in a water matrix with mixing. This mixture is an industry standard, but does not simulate in-situ conditions. In-situ conditions have a soil water mixture of approximately 5.8:1, assuming 30% porosity. In addition, the soil particles are compacted and mixing is impossible.

In-situ conditions present a unique set of obstacles to remediation implementation. Remediation is much more complex than bench study chemistry. Remediation requires the combination of injection pressures, volumes and flow rates; reagent type and concentration; and injection location spacing to achieve a uniform (as much as possible) distribution of reagents. Injectable reagent volumes are very site specific depending on grain size, degree of inter-bedded soil types, depth to water and previous penetrations. In general, reagent volumes are limited to 5-10% of a pore volume to prevent surfacing (escape of reagents from the subsurface to the ground). A deep saturated zone comprised of homogeneous gravel will accept a higher volume of reagent, but those conditions are rare. Oxidant concentrations are generally limited to less than 20% due to health and safety concerns regarding handling and surfacing.

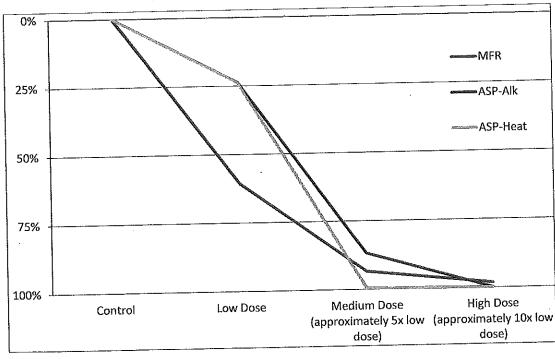
#### **Remediation Recommendations**

One observation of the bench study data is unique and important. The reduction in concentration in both solid and aqueous phases was very limited in both low-dose persulfate applications, while the MFR low-dose application showed a 61% and 74% VOC reduction for aqueous and solid phase, respectively (See graphs below).

### Percent EDC Reduction, Solid Phase



#### Percent EDC Reduction, Aqueous Phase



In-Situ Oxidative Technologies, Inc.

Based on the discussion above regarding injectable volumes and concentrations, field applications at the site will mimic low-dose applications. Total contaminant mass reduction comes from a cumulative effect of multiple low-dose applications, as opposed to one large medium-dose application. It does not appear that multiple low-dose applications of activated persulfate will lead to a cumulative mass reduction, since individual low-dose applications are relatively ineffective. However, multiple low-dose applications of MFR should produce a cumulative mass reduction.

Based on the results of the bench study and the inherent application limitations, ISOTEC recommends a field pilot test utilizing MFR as the oxidant.

# ISOTEC ....

**TABLES** 

In-Situ Oxidative Technologies, Inc.

# Table 1. Initial Characterization PBW/Formosa Plastics, Point Comfort, Texas ISOTEC Project #901132

Sample ID Matrix	P-56 Aqueous		Soil Comp Soil
VOCs	(ug/l)		(mg/kg)
Vinyl chloride	13,300	1	ND<0.298
1,1-Dichloroethene (1,1-DCE)	1,780	ļ	ND<0.298
trans-1,2-Dichloroethene	4,140		ND<0.298
1,1-Dichloroethane (1,1-DCA)	8,400	ļ	ND<0.298
cis-1,2-Dichloroethene	2,650	İ	ND<0.298
Chloroform	81,600		2.1
1,2-Dichloroethane (EDC)	1,280,000	D	44.9
Benzene	2,920		ND<0.298
Trichloroethene	4,590		ND<0.298
1,1,2-Trichloroethane	7,330		0.404
Tetrachloroethene	2,070		ND<0.298
Total VOCs (ug/l)	1,408,780		47.4
Other Parameters	(ug/l)		(mg/kg)
Alkalinity	606,000		NA
Nitrate	ND<500		NA
Sulfate as SO4	378,000		NA
Total Organic Carbon (TOC)	8,540		1190
Total Dissolved Solids (TDS)	9,150,000		NA NA
Ferrous Iron	4,960		NA
Iron	8,710		5,640
Manganese	7,930		136

#### Note:

 $\overline{\text{ug/l}}$  = micrograms per liter. mg/kg = milligrams per kilogram

ND = Compound was analyzed for but not detected at the reporting limit (RL) indicated by the number following "<".

NA = Compound was not analyzed for.

D = The reported value is from a diluted analysis.

# Table 2. Treatability Study Results (MFR) PBW/Formosa Plastics, Point Comfort, Texas ISOTEC Project #901132

Sample ID	M/Control		M/T-A	М/Т-В		M/T-C	
Catalyst Used	none		Cat-4260	Cat-4260		Cat-4260	
Oxidant Used	none		H2O2	H2O2		H2O2	
Oxidant Added (by weight)	0		6.6 g/kg	33.3 g/kg		66 g/kg	
VOCs (ug/l)			Aqueo	us Phase			
Vinyl chloride	2,760		ND<1000	ND<250		ND<50	
trans-1,2-Dichloroethene	1,520	J	ND<1000	ND<250		ND<50	
1,1-Dichloroethane (1,1-DCA)	2,990		1,120	ND<250		ND<50	
cis-1,2-Dichloroethene	ND<2500		ND<1000	ND<250		ND<50	
Chloroform	37,200		20,500	3,770		2,070	ļ
1,2-Dichloroethane (EDC)	470,000		185,000	30,600		8,190	
Benzene	ND<2500		ND<1000	ND<250		ND<50	
Trichloroethene	1,690	J	ND<1000	ND<250		ND<50	
1,1,2-Trichloroethane	3,730		2,140	744		416	
Total VOCs (ug/l)	519,890		208,760	35,114		10,676	
EDC reduction	-		60.64%	93.49%		98.26%	
VOC reduction	-		59.85%	93.25%		97.95%	
							_
VOCs (mg/kg)	,		Solid	Phase			
cis-1,2-Dichloroethene	ND<0.635		ND<0.124	ND<0.00121		ND<0.00125	
Chloroform	2.54		0.779	ND<0.00121		ND<0.00125	
1,2-Dichloroethane (EDC)	64.10		16.70	0.011		0.0063	
1,1,2-Trichloroethane	0.43	J	0.18	0.0005	J	0.0005	J
Total VOCs (mg/kg)	67.1		17.7	0.01		0.01	
EDC reduction	-		73.95%	99.98%		99.99%	
VOC reduction	-		73.66%	99.98%		99.99%	
Other Parameters							
ferrous Iron (ug/l)	ND<40.0		ND<40.0	ND<40.0		ND<40.0	
Final pH value (SU)	6.51		6.63	6.90		7.15	
Final ORP value (mV)	185		182	189		203	
Final TDS value (ppm)	5,940		6,286	8,220		11,070	

#### Note:

ug/l = micrograms per liter, mg/kg = milligrams per kilogram, g/kg = grams per kilogram, mV = milli volts. ND = Compound was analyzed for but not detected at the reporting limit (RL) indicated

J = The concentration was detected at a value below the RL and above the method detection limit (MDL). Total oxidant demand is presented as g/kg (grams of oxidant per kilogram of soil).

by the number following "<".

Table 3. Treatability Study Results (ASP-Alk) PBW/Formosa Plastics, Point Comfort, Texas ISOTEC Project #901132

Sample ID	S-A/Control		S-A/A		S-A/B		S-A/C	
Catalyst Used	none		NaOH		NaOH		NaOH	
Oxidant Used	none		Na <sub>2</sub> S <sub>2</sub> O <sub>8</sub>	İ	$Na_2S_2O_8$		$Na_2S_2O_8$	
Oxidant Added (by weight)	· <b>o</b>		6 g/kg		30 g/kg		60 g/kg	
			Agu	eou:	s Phase			
VOCs (ug/l) Vinyl chloride	ND<5000		3,010	J	3,700		396	
trans-1,2-Dichloroethene	ND<5000		ND<5000		260	J	9.24	
1,1-Dichloroethane (1,1-DCA)	2,720	J	1,910	J	539		3.42	J
	ND<5000		ND<5000		185	J	11.20	
cis-1,2-Dichloroethene	.41,600	1	22,300		1,710		ND<5.0	
Chloroform	652,000		497,000		86,100		243	
1,2-Dichloroethane (EDC)	ND<5000		ND<5000		ND<500		1.35	J
Benzene	ND<5000		ND<5000		211	J	2.14	J
Trichloroethene	4,370	J	ND<5000		ND<500		ND<5.0	
1,1,2-Trichloroethane	4,370 ND<5000	,	ND<5000		183	J	1.51	J
Tetrachloroethene	i		524,220		92,888		667.86	
Total VOCs (ug/l)	700,690	l	23.77%		86.79%		99.96%	
EDC reduction	7		25.19%		86.74%		99.90%	
VOC reduction	-		23.13%		00.7470			
VOCs (mg/kg)			S	olid	Phase			
Vinyl chloride	ND<0.611		ND<0.624		0.551		ND<0.121	
1,1-Dichloroethane	0.416	J	0.469	J	0.076	J	ND<0.121	
Chloroform	5.41	-	4,54		0.201		ND	
1,2-Dichloroethane (EDC)	116		124		12.8		0.063	J
1,1,2-Trichloroethane	0.697		ND<0.624		ND<0.125		ND<0.121	
Total VOCs (mg/kg)	122.52		129.01		13.63		0.06	
			increase		88.97%		99.95%	
EDC reduction	_		increase		88.88%		99.95%	
VOC reduction	_							
1/ Ovident Concumption	_		57%		30%		26%	
% Oxidant Consumption			3.42		9.00		15.60	
Total Oxidant Demand (g/kg)								
Other Parameters								
Final pH value (SU)	6.6		11.36		12.06		12.25	
Final ORP value (mV)	46		-159		-199		-211	
Final TDS value (ppm)	10,880		18,340		48,500		91,740	

ug/l = micrograms per liter, mg/kg = milligrams per kilogram, g/kg = grams per kilogram, mV = milli volts. ND = Compound was analyzed for but not detected at the reporting limit (RL) indicated by the number following "<" J = The concentration was detected at a value below the RL and above the method detection limit (MDL).

Total oxidant demand is presented as g/kg (grams of oxidant per kilogram of soil).

Table 4. Treatability Study Results (ASP-Heat) PBW/Formosa Plastics, Point Comfort, Texas ISOTEC Project #901132

Sample ID	S-H/Control		S-H/A		S-H/B		S-H/C	
Catalyst Used	Heat (60°C)		Heat (60°C)		Heat (60°C)		Heat (60°C)	
Oxidant Used	none		$Na_2S_2O_8$		$Na_2S_2O_8$		$Na_2S_2O_8$	
Oxidant Added (by weight)	0		6 g/kg		30 g/kg		60 g/kg	
VOCs (ug/l)			Aqı	ieou	s Phase			
Chloromethane	ND<5000		ND<5000		1,150	l	571	
Methylene chloride	ND<10000		ND<10000		9,420	١	4,490	
1,1-Dichloroethane (1,1-DCA)	3,280	յ	2,800	J	211		64,80	J
Chloroform	50,900		38,100		15,400		8,210	
1,1,1-Trichloroethane (1,1,1-TCA)	ND<5000		ND<5000		143		107	
Carbon tetrachloride	ND<5000		ND<5000		133	1	109	
1,2-Dichloroethane (EDC)	746,000		568,000		2,750	•	200	
Trichloroethene (TCE)	1,680	J	ND<5000		ND<100		ND<100	
Bromodichloromethane	ND<5000		ND<5000		168		89.10	J
1,1,2-Trichloroethane (1,1,2-TCA)	4,860	J	3,340	J	8,310		2,650	
Tetrachloroethene (PCE)	ND<5000		ND<5000		28.1	J	ND<100	
1,1,2,2-Tetrachloroethane	ND<5000		ND<5000		659		410	
Total VOCs (ug/l)	806,720		612,240		38,372		16,901	
EDC reduction	-		23.86%		99.63%		99.97%	
VOC reduction	-		24.11%		95.24%		97.90%	
VOCs (mg/kg)			S	olid	Phase			
Methylene chloride	ND<1.22		ND<1.22		0.549		0.372	
Chloroform	2.75		2.90		0.553		0.409	
1,2-Dichloroethane (EDC)	74.00		75.00		0.487		0.053	J
1,1,2-Trichloroethane	0.491	J	0,503	J	0.585		0.176	
Total VOCs (mg/kg)	77.24		78.40		2.17		1.01	
EDC reduction	-		increase		99.34%		99.93%	
VOC reduction	-		increase		97.19%		98.69%	
% Oxidant Consumption	-		72%		63%		53%	
Total Oxidant Demand (g/kg)	-		4.32		18.90		31.80	
Other Parameters								
Final pH value (SU)	6.57		6.18		6.02		5.37	
Final ORP value (mV)	34		48		57		99	
Final TDS value (ppm)	11,170		19,040		36,150		55,300	

#### Note:

ug/l = micrograms per liter, mg/kg = milligrams per kilogram, g/kg = grams per kilogram, mV = milli volts.

ND = Compound was analyzed for but not detected at the reporting limit (RL) indicated by the number following "<".

J = The concentration was detected at a value below the RL and above the method detection limit (MDL).

Total oxidant demand is presented as g/kg (grams of oxidant per kilogram of soil).



# **ATTACHMENTS**

(ATTACHMENT A: LABORATORY ANALYTICAL DATA PACKAGES)

In-Situ Oxidative Technologies, Inc.



for Isotec 11 Princess Road Suite A

Lawrenceville, NJ 08648

Lab Case Number: E12-09138

Project Name: PB&W/FORMOSA PLASTICS - 901132

RL = REPORTING LIMIT

#### MDL = METHOD DETECTION LIMIT

#### Volatiles

Lab ID: 09138-001 Client ID: P-56

Matrix-Units: Aqueous-ug/L

Percent Moisture: 100

Date Sampled: 9/10/2012 Time Sampled: 14:00 Date Analyzed: 9/12/12

Compound	Conc	Q	$\mathbf{RL}$	MDL	
Chloromethane	ND		1000	440	
Vinyl chloride	13300		1000	580	
Bromomethane	ND		1000	580	
Chloroethane	ND		1000	620	
Trichlorofluoromethane	ND		1000	640	
Acrolein	ND		20000	4640	
1,1-Dichloroethene	1780	j.ee	1000	680	
Methylene chloride	ND		4000	3960	
Acrylonitrile	ND		20000	3880	
tert-Butyl alcohol (TBA)	ND		2000	1720	
trans-1,2-Dichloroethene	4140		1000	600	
Methyl tert-butyl ether (MTBE)	ND		1000	460	
1,1-Dichloroethane	8400		1000	440	
cis-1,2-Dichloroethene	2650		1000	440	
Chloroform	81600		1000	520	
1,1,1-Trichloroethane	ND		1000	500	
Carbon tetrachloride	ND		1000	540	
1,2-Dichloroethane (EDC)	1280000	D	10000	5800	
Benzene	2920		1000	460	
Trichloroethene	4590		1000	540	
1,2-Dichloropropane	ND		1000	440	
Bromodichloromethane	ND		1000	420	
2-Chloroethyl vinyl ether	ND ·		1000	660	
cis-1,3-Dichloropropene	ND		1000	500	
Tohiene	ND		1000	660	

ND = Analyzed for but Not Detected at the MDL

D = The compound was reported from the Diluted analysis

Continued on next page

273 Franklin Road Randolph, NJ 07869 Phone: 973 361 4252 Fax: 973 989 5288





for

**Isotec** 11 Princess Road

Suite A

Lawrenceville, NJ 08648

Project Name: PB&W/FORMOSA PLASTICS - 901132 Lab Case Number: E12-09138

RL = REPORTING LIMIT

#### MDL = METHOD DETECTION LIMIT

#### Volatiles

Lab ID: 09138-001 Client ID: P-56

Matrix-Units: Aqueous-ug/L Percent Moisture: 100

Date Sampled: 9/10/2012 Time Sampled: 14:00

Date Analyzed: 9/12/12

Compound	Conc	Q	RL	MDL	
	ND		1000	580	
trans-1,3-Dichloropropene	7330		1000	600	
1,1,2-Trichloroethane	2070		1000	420	
Tetrachloroethene			1000	680	
Dibromochloromethane	ND		- • •	480	
Chlorobenzene	ND		1000		
Ethylbenzene	ND		1000	620	
Total Xylenes	ND		2000	1720	
Bromoform	ND		1000	460	
1,1,2,2-Tetrachloroethane	ND		1000	460	
	ND		1000	420	
1,3-Dichlorobenzene	ND		1000	480	
1,4-Dichlorobenzene	ND		1000	480	
1,2-Dichlorobenzene			1000		-
TOTAL VO's:	1380000				=

#### General Analytical

Lab ID: 09138-001 Client ID: P-56

Percent Moisture: 100

Date Sampled: 9/10/2012 Time Sampled: 14:00

Davamatan	Result	RL	MDL	Matrix-Units	Date Analyzed
Parameter Alkalinity Nitrate	606000 ND	8000 500	4400 299	Aqueous-ug/L Aqueous-ug/L	9/12/2012 12:00 9/11/2012 12:36
Sulfate as SO4	378000	125000	38500	Aqueous-ug/L	9/13/2012 12:15 9/19/2012 8:45
Total Organic Carbon	8540	1000 1250000	460 175000	Aqueous-ug/L Aqueous-ug/L	9/11/2012 10:00
Total Dissolved Solids Ferrous Iron	9150000 4960	200	40.0	Aqueous-ug/L	9/12/2012 16:45

ND = Analyzed for but Not Detected at the MDL

273 Franklin Road Randolph, NJ 07869 Phone: 973 361 4252 Fax: 973 989 5288





for

Isotec

11 Princess Road

Suite A

Lawrenceville, NJ 08648

Project Name: PB&W/FORMOSA PLASTICS - 901132 Lab Case Number: E12-09138

#### RL = REPORTING LIMIT

#### MDL = METHOD DETECTION LIMIT

#### Volatiles

Lab ID: 09138-002 Client ID: SOIL COMP Matrix-Units: Soil-mg/Kg Percent Moisture: 16.1

Date Sampled: 9/10/2012 Time Sampled: 14:00 Date Analyzed: 9/19/12

Compound	Conc	Q	RL	MDL
	ND		0.298	0.068
Chloromethane	ND		0.298	0.197
Vinyl chloride	ND		0.298	0.164
Bromomethane	ND		0.298	0.125
Chloroethane	ND		0.298	0.140
Trichlorofluoromethane	ND		5.96	0.709
Acrolein	ND		0.298	0.247
1,1-Dichloroethene			0.596	0.590
Methylene chloride	ND		5.96	0.468
Acrylonitrile	ND		0.596	0.218
tert-Butyl alcohol (TBA)	ND		0.298	0.152
trans-1,2-Dichloroethene	ND		0.298	0.083
Methyl tert-butyl ether (MTBE)	ND		0.298	0.122
1,1-Dichloroethane	ND		0.298	0.110
cis-1,2-Dichloroethene	ND		0.298	0.110
Chloroform	2.10		0.298	0.140
1,1,1-Trichloroethane	ND		0.298	0.212
Carbon tetrachloride	ND		0.298	0.072
1,2-Dichloroethane (EDC)	44.9			0.072
Benzene	ND		0.298	0.072
Trichloroethene	ND		0.298	0.143
1,2-Dichloropropane	ND		0.298	
Bromodichloromethane	ND		0.298	0.092
2-Chloroethyl vinyl ether	ND .		0.298	0.104
cis-1,3-Dichloropropene	ND		0.298	0.078
Toluene	ND		0.298	0.068
trans-1,3-Dichloropropene	ND		0.298	0.066

ND = Analyzed for but Not Detected at the MDL Continued on next page

273 Franklin Road Randolph, NJ 07869 Phone: 973 361 4252 Fax: 973 989 5288





for **Isotec** 11 Princess Road Suite A Lawrenceville, NJ 08648

Project Name: PB&W/FORMOSA PLASTICS - 901132 Lab Case Number: E12-09138

RL = REPORTING LIMIT		Ŋ	MDL = M	ETHOD DETE	CTION LIMIT
TO TO THE PARTY OF	Volatiles	3			
Lab ID: 09138-002 Client ID: SOIL COMP Matrix-Units: Soil-mg/Kg Percent Moisture: 16.1				Date Sample Time Sample Date Analyz	ed: 14:00
Compound		Conc	Q	RL	MDL
1,1,2-Trichlor Tetrachloroeti Dibromochlor Chlorobenzen Ethylbenzene Total Xylenes Bromoform 1,1,2,2-Tetrac 1,3-Dichlorol 1,2-Dichlorol TOTAL VO	hene romethane se chloroethane penzene penzene penzene	0.404 ND ND ND ND ND ND ND ND ND ND ND ND ND		0.298 0.298 0.298 0.298 0.298 0.596 0.298 0.298 0.298 0.298	0.080 0.149 0.092 0.098 0.107 0.206 0.068 0.072 0.098 0.083 0.098
	Metals	3			
Lab ID: 09138-002 Client ID: SOIL COMP Matrix-Units: Soil-mg/Kg Percent Moisture: 16.1				Time Samp	ed: 9/10/2012 Ied: 14:00 zed: 9/14/12
Parameter		Result	Q	RL	MDL
Iron Manganese		5640 136		31.8 1.27	15.9 0.318

ND = Analyzed for but Not Detected at the MDL

Manganese







for

Isotec

11 Princess Road

Suite A

Lawrenceville, NJ 08648

Project Name: PB&W/FORMOSA PLASTICS - 901132

Lab Case Number: E12-09138

RL = REPORTING LIMIT				MDL = METHOD DE	TECTION LIMIT
	G	General Ana	lytical		
Lab ID: 09138-002 Client ID: SOIL COMP Percent Moisture: 16.1				-	oled: 9/10/2012 pled: 14:00
Parameter	Result	RL	MDL	Matrix-Units	Date Analyzed
Total Organic Carbon	1190	1000	376	Soil-mg/Kg	9/18/2012 9:15
		Metals	)	,	
Lab ID: 09138-003 Client ID: P-56 FILT. Matrix-Units: Aqueous-ug/L Percent Moisture: 100				Time Sam	pled: 9/10/2012 pled: 14:00 yzed: 9/12/12

Parameter

Manganese

Iron

Result

8710

7930

These data have been reviewed and accepted by:

Q

Michael H. Leftin, Ph.D

RL

100

4.00

Laboratory Director

MDL

50.0

2.00



# Integrated Analytical Labs 273 Franklin Road Pandolph, NJ 07869

Web: www.ialonline.com

CUSTOMER INFO		PORTIN	iG INFO		Tur	naround	Time (s	tarts the	following	day if s	amples re	'd a	u lab >	DEW)		TO THE	NOT	CHIA	ANT	red Ted
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# PROJECT INFORMATION



Case No. E12-09138 Project PB&W/FORMOSA P	PLASTICS - 901132
The state of the s	P.O.# 4254
Customer Isotec  Contact Prasad Kakarla	Received 9/10/2012 16:11
EMail EDDs	Verbal Due 9/24/2012
ychin@insituoxidation.com Phone (609) 275-8500 Fax 1(609) 275-9608	Report Due 10/1/2012
Report To	<u>Bill To</u>
11 Princess Road	11 Princess Road
Suite A	Suite A
Lawrenceville, NJ 08648	Lawrenceville, NJ 08648
Attn: Prasad Kakaria	Attn: Prasad Kakarla
Report Format Result Only	
Additional Info State Form Field Sampling	Conditional VOA
Lab ID         Client Sample ID         Depth Top / Bottom           09138-001         P-56         n/a           09138-002         SOIL COMP         n/a           09138-003         P-56 FILT.         n/a	Sampling Time   Matrix   Unit   # of Containers
Sample # Tests Status	QA Method
001 PP VO + Cis 1,2-DCE + MTBE .TBA In Process  Metals Filtration Complete  Alkalinity Run	and the court of the court of the Court ( Addition ) and the court of the Court o
" Ferrous (II) Iron Run " NO3 (Nitrate) Run	4500NO3F
" Sulfate (SO4) Run " TDS (Dissolved) Run	2540C
" TOC Run 002 PP VO + Cis 1,2-DCE + MTBE TBA Run	5310¢ 8260B
Iron - Fe  Manganese - Mn  Run	6020 6020
" TOC Run	Mod Lloyd Kahn
003 Iron - Fe In Process  Manganese - Min In Process	
00/11/2012 08:54 by Filen - NOTE 1	

09/11/2012 08:54 by Ellen - NOTE 1

SOIL VO CONTENTS: 20g SOIL/20ml MEOH

09/11/2012 13:12 by Mark - NOTE 2

USE LOWEST MDL'S POSSIBLE

# PROJECT INFORMATION



Case No. E12-09138

Project PB&W/FORMOSA PLASTICS - 901132

09/12/2012 16:26 by melissa - REV 1

AS PER YAN CHIN, RUN SAMPLE 001 FOR FERROUS IRON.

# INTEGRATED ANALYTICAL LABORATORIES, LLC

# SAMPLE RECEIPT VERIFICATION

CASE NO: E 12 09138 CLIENT: TSOTEC	
COOLER TEMPERATURE: 2° - 6°C: (See Chain of Custody) Comments	
COC: COMPLETE / INCOMPLETE	,
✓ = YES/NA × = NO	
✓ Bottles Intact ✓ no-Missing Bottles ✓ no-Extra Bottles	
✓ Sufficient Sample Volume  ✓ no-headspace/bubbles in VOs  ✓ Labels intact/correct  ✓ pH Check (exclude VOs) <sup>1</sup>	
✓ Correct bottles/preservative ✓ Sufficient Holding/Prep Time	
Sample to be Subcontracted  ✓ Chain of Custody is Clear	
All samples with "Analyze Immediately" holding times will be analyzed by this laboratory past the holding time. This includes but is not limited to the following tests: pH, Temperature, Free Residual Chlorine, Total Residual Chlorine, Dissolved Oxygen, Sulfite.  ADDITIONAL. COMMENTS:  SAMPLE(S) VERIFIED BY: INITIAL DATE PIOLIZ  CORRECTIVE ACTION REQUIRED: YES SELOW)	
If COC is NOT clear, <u>STOP</u> until you get client to authorize/clarify work.	
CLIENT NOTIFIED: PROJECT CONTACT: SUBCONTRACTED LAB: DATE SHIPPED: ADDITIONAL COMMENTS:	
VERIFIED/TAKEN BY: INITIAL DATE 9.11./2 REVIOUS 2000年發写13	3

# Laboratory Custody Chronicle

IAL Case No.

E12-09138

Client Isotec

Project

PB&W/FORMOSA PLASTICS - 901132

Received On

9/10/2012@16:11

Department: Volatiles PP VO + Cis 1,2-DCE + MTBE & TBA	09138-001 -002	Aqueous Soil	<u>Prep. Date</u> n/a n/a	<u>Analvst</u> n/a n/a	<u>Analysis Date</u> 9/12/12 9/19/12	<i>Analyst</i> Sylvia Mei
Department: Metals Iron - Fe " Manganese - Mn "	-002 -003 -002 -003	Soil Aqueous Soil Aqueous	Prep. Date 9/13/12 9/12/12 9/13/12 9/12/12	Analyst Lisa Lisa Lisa Lisa	<u>Analysis Date</u> 9/14/12 9/12/12 9/14/12 9/12/12	Analyst En En En En En
Department: Wet Chemistry Alkalinity Ferrous (II) Iron NO3 (Nitrate) Sulfate (SO4) TDS (Dissolved) TOC	-001	Aqueous	Prep. Date n/a n/a n/a n/a n/a n/a n/a n/a n/a n/a	Analyst n/a n/a n/a n/a n/a n/a n/a n/a n/a	Analysis Date 9/12/12 9/12/12@16:45 9/11/12@12:36 9/13/12 9/11/12 9/19/12 9/18/12	Analyst Kris Kris Geeta Debbie Robert Elma Elma



Isotec 11 Princess Road Suite A Lawrenceville, NJ 08648

Project Name: PB&W/FORMOSA PLASTICS - 901132

IAL Case Number: E12-09359

These data have been reviewed and accepted by:

Michael H. Lefth, Ph.D.

Laboratory Director

This report shall not be reproduced, except in its entirety, without the written consent of Integrated Analytical Laboratories, LLC. The test results included in this report relate only to the samples analyzed.



# Sample Summary

LAL Case No.

E12-09359

Client Isotec

Project PB&W/FORMOSA PLASTICS - 901132

Received On 9/14/2012@17:30

- Automotive Control					<u># of</u>
<u>Lab ID</u> 09359-001 09359-002 09359-003 09359-004 09359-005 09359-006 09359-007 09359-008	Client Sample ID M/CONTROL M/A M/B M/C M/CONTROL M/A M/B M/C	Depth Top/Bottom  n/a  n/a  n/a  n/a  n/a  n/a  n/a  n/	Sampling Time 9/14/2012 9/14/2012 9/14/2012 9/14/2012 9/14/2012 9/14/2012 9/14/2012 9/14/2012	Matrix Aqueous Aqueous Aqueous Aqueous Soil Soil Soil	<u>Container</u> 2 2 2 2 1 1 1

# INTEGRATED ANALYTICAL LABORATORIES, LLC.

#### TABLE OF CONTENTS

•	<u>Page</u>
Qualifiers Results Summary Report Analytical Results	1 3
Volatiles General Analytical Ferrous (II) Iron	
Sample Tracking Chains of Custody Project Information Sample Receipt Verification Laboratory Chronicle	12
Last Page of the Report	<sub>.</sub> 16
This report was finalized on October 02, 2012	

<sup>\*</sup> Methodology is included in the IAL Project Information Page

#### INTEGRATED ANALYTICAL LABORATORIES, LLC.

#### **DEFINITIONS / QUALIFIERS**

#### DATA QUALIFIERS

- <u>B</u> Indicates the analyte was found in the associated method blank as well as in the sample. It indicates probable laboratory contamination.
- C Indicates analyte is a common laboratory contaminant.
- **D** Indicated analyte was reported from diluted analysis.
- E Identifies a compound concentration that exceeds the upper level of the calibration range of the instrument for that specific analysis.
- <u>J</u> Indicates an estimated value. This flag is used when the concentration in the sample is below the RL but above the MDL.

#### REPORTING DEFINITIONS

- RL Reporting Limit. The RL is determined by the lowest concentration in the calibration curve. For most Wet Chemistry methods, the RL is defined by using the PQL.
- MDL Method Detection Limit as determined according to 40CFR Part 136 Appendix B.
- PQL Practical Quantitation Limit. Usually defined as a value 3-5 times the MDL.
- ND Indicates analyte was analyzed for but not detected above the MDL.
- **DF** Dilution Factor
- LCS Laboratory Control Sample
- **LCSD** Laboratory Control Sample Duplicate
  - MS Matrix Spike
  - MSD Matrix Spike Duplicate
- <u>DUP</u> Duplicate

# INTEGRATED ANALYTICAL LABORATORIES, LLC.

#### SUMMARY REPORT

#### Client: Isotec

Project: PB&W/FORMOSA PLASTICS - 901132

Lab Case No.: E12-09359

		I	Jab Caș€	No.: E12-	19359	التكنيسية والمستوارية				0.0.1
Lab ID: 09359-001		09359-002			09359-003		09359-004			
Client ID:	M/CONTROL		M/A			M/B		M/C		
Matrix:	Aqueous		Aqueous			Aqueous		Aqueous		
Sampled Date	9/14/12		9/14/12		9/14/12		9/14/12			
~ 1			MDL	Conc	Q MDL	Conc	Q_	MDL	Conc (	Q MDL
PARAMETER(Units)						<i></i>	/L-p	n.b.)	(ug/L	-onb)
Volatiles (Units)	(ug	/L-ppl	b)	(ug/L	-ppb)	(ug	γ <b></b> μ,		· -	
ĭ	2760		1600	ND	640	ND		160	ND	32.0
Vinyl chloride	ND		3450	ND	1380	ND		345	ND	69.0
tert-Butyl alcohol (TBA)			1150	ND	460	ND		115	ND	23.0
trans-1,2-Dichloroethene	ND		1350	ND	540	ND		135	ИD	27.0
Methyl tert-butyl ether (MTBE)	2990		1300	1120	520	ND		130	ND	26.0
1,1-Dichloroethane	2990 ND		1300	ND	520	ND		130	ND	26.0
cis-1,2-Dichloroethene			1300	20500	520	3770		130	2070	26.0
Chloroform	37200		1850	185000	740	30600		185	8190	37.0
1,2-Dichloroethane (EDC)	470000			ND	460	ND		115	ND	23.0
Trichloroethene	1690	J	1150	2140	560	744		140	416	28.0
1,1,2-Trichloroethane	3730		1400	2140	300	1		···		
	520000	т		209000		35100			10700	
TOTAL VO's:	320000			1						
General Analytical (Units)										40.0
Ferrous (II) Iron(ug/L)	ND		40.0	ND	40.0	ND		40.0	ND	40.0
Lab ID:		359-(	05	0935	59-006	09		-007		59-008
Client ID:	1		ROL	N	I/A		M/	\$		I/C
Matrix:	1	Soil		5	Soil	}	So			Soil
Sampled Date	1 .	9/14/1		9/1	14/12		9/14			14/12
4	Conc		MDL	Conc	Q MDL	Conc	_Q	MDL	Conc	Q MDL
PARAMETER(Units)	<del>                                     </del>		, <u>.</u>	(ma/l	(g-ppm)	(m	e/Ke	-ppm)	(mg/l	(g-ppm)
Volatiles (Units)	(mg	g/Kg-p	pm)			1	eo		ND	0.00114
tert-Butyl alcohol (TBA)	ND		0.463	ND	0.090	ND		0.0011	ND	0.00028
Methyl tert-butyl ether (MTBE)	ND		0.178	ND	0.035	ND		0.000278		0.00028
cis-1,2-Dichloroethene	ND		0.235	ND	0.046	ND		0.000375	ND	0.00036
	2.54		0.235	0.779	0.046	ND		0.000351	ND	
Chloroform 1,2-Dichloroethane (EDC)	64.1		0.152	16.7	0.030	0.011		0.000254	0.00632	0.00026
	0.428	J	0.171	0.184	0.034	0.00050	)2 J	0.000242	0.000455	J 0.00025
1,1,2-Trichloroethane	1								0.00678	Ť
TOTAL VO's:	67.1	J		17.7		0.012	J		1 0.00078	3
SSELUIAL YUS.										

ND = Analyzed for but Not Detected at the MDL

I = The concentration was detected at a value below the RL and above the MDL

All qualifiers on individual Volatiles & Semivolatiles are carried down through summation.

### INTEGRATED ANALYTICAL LABORATORIES

#### VOLATILE ORGANICS

Lab ID: 09359-001 Client ID: M/CONTROL Date Received: 09/14/2012 Date Analyzed: 09/17/2012

Data file: E5430.D

GC/MS Column: DB-624 Sample wt/vol: 0.001mL

Matrix-Units: Aqueous-μg/L (ppb)

Dilution Factor: 5000 % Moisture: 100

Compound	Concentration	Q	RL	MDL
Chloromethane	ND		2500	2450
Vinyl chloride	2760		2500	1600
Bromomethane	ND		2500	2450
Chloroethane	ND		2500	2000
Trichlorofluoromethane	ND		2500	1500
	ND		50000	12600
Acrolein	ND		2500	1400
1,1-Dichloroethene	ND	•	10000	9900
Methylene chloride	ND		50000	9050
Acrylonitrile	ND		5000	3450
tert-Butyl alcohol (TBA)	1520	J	2500	1150
trans-1,2-Dichloroethene	ND	•	2500	1350
Methyl tert-butyl ether (MTBE)	2990		2500	1300
1,1-Dichloroethane	ND		2500	1300
cis-1,2-Dichloroethene	37200		2500	1300
Chloroform	ND		2500	1350
1,1,1-Trichloroethane	ND		2500	1350
Carbon tetrachloride	470000		2500	1850
1,2-Dichloroethane (EDC)	470000 ND		2500	1450
Benzene	1690	J	2500	1150
Trichloroethene		J	2500	1300
1,2-Dichloropropane	ND		2500	1150
Bromodichloromethane	ND		2500	2250
2-Chloroethyl vinyl ether	ND		2500	1200
cis-1,3-Dichloropropene	ND		2500	850
Toluene	ND		2500	1600
trans-1,3-Dichloropropene	ND			1400
1,1,2-Trichloroethane	3730		2500	1100
Tetrachloroethene	ND		2500	2050
Dibromochloromethane	ND		2500	2030 1350
Chlorobenzene	ND		2500	1300
Ethylbenzene	ND		2500	3300
Total Xylenes	ND		5000	
Bromoform	ND	•	2500	2250
1,1,2,2-Tetrachloroethane	ND		2500	2150
1,3-Dichlorobenzene	ND		2500	2450
1,4-Dichlorobenzene	ND		2500	2450
1,2-Dichlorobenzene	ND		2500	2300

Total Target Compounds (37):

520000

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## **VOLATILE ORGANICS**

Lab ID: 09359-002 Client ID: M/A

Date Received: 09/14/2012 Date Analyzed: 09/17/2012

Data file: E5447.D

GC/MS Column: DB-624 Sample wt/vol: 0.0025mL

Matrix-Units: Aqueous-μg/L (ppb)

Dilution Factor: 2000 % Moisture: 100

Compound	Concentration	Q	RL	MDL
Chloromethane	ND	······································	1000	980
Vinyl chloride	ND		1000	640
Bromomethane	ND		1000	980
Chloroethane	ND		1000	800
Trichlorofluoromethane	ND		1000	600
Acrolein	ND		20000	5020
1,1-Dichloroethene	ND		1000	560
Methylene chloride	ND		4000	3960
Acrylonitrile	ND		20000	3620
tert-Butyl alcohol (TBA)	ND		2000	1380
trans-1,2-Dichloroethene	ND		1000	460
Methyl tert-butyl ether (MTBE)	ND		1000	540
1,1-Dichloroethane	1120		1000	520
cis-1,2-Dichloroethene	ND		1000	520
Chloroform	20500		1000	520
1,1,1-Trichloroethane	ND		1000	540
Carbon tetrachloride	ND		1000	540
1,2-Dichloroethane (EDC)	185000		1000	740
Benzene	ND		1000	580
Trichloroethene	ND		1000	460
1,2-Dichloropropane	ND		1000	520
Bromodichloromethane	ND		1000	460
2-Chloroethyl vinyl ether	ND		1000	900
cis-1,3-Dichloropropene	ND		1000	480
Toluene	ND		1000	340
	ND		1000	640
trans-1,3-Dichloropropene	2140		1000	560
1,1,2-Trichloroethane Tetrachloroethene	ND		1000	440
Dibromochloromethane	ND		1000	820
	ND		1000	540
Chlorobenzene	ND		1000	520
Ethylbenzene Tatal Valence	ND		2000	1320
Total Xylenes	ND		1000	900
Bromoform	ND		1000	860
1,1,2,2-Tetrachloroethane	ND		1000	980
1,3-Dichlorobenzene	ND		1000	980
1,4-Dichlorobenzene	ND		1000	920
1,2-Dichlorobenzene	1412			

Total Target Compounds (37):

209000

## VOLATILE ORGANICS

Lab ID: 09359-003 Client ID: M/B

Date Received: 09/14/2012 Date Analyzed: 09/17/2012

Data file: E5448.D

GC/MS Column: DB-624 Sample wt/vol: 0.01mL

Matrix-Units: Aqueous-μg/L (ppb)

Dilution Factor: 500 % Moisture: 100

Сотроинд	Concentration	Q	RL	MDL
Chloromethane	ND		250	245
Vinyl chloride	ND		250	160
Bromomethane	ND		250	245
Chloroethane	ND		250	200
Trichlorofluoromethane	ND		250	150
Acrolein	ND		5000	1260
1,1-Dichloroethene	ND		250	140
Methylene chloride	ND		1000	990
Acrylonitrile	ND		5000	905
tert-Butyl alcohol (TBA)	ND		500	345
trans-1,2-Dichloroethene	ND		250	115
Methyl tert-butyl ether (MTBE)	ND		250	135
1,1-Dichloroethane	ND		250	130
cis-1,2-Dichloroethene	ND		250	130
Chloroform	3770		250	130
1,1,1-Trichloroethane	ND		250	135
Carbon tetrachloride	ND		250	135
1,2-Dichloroethane (EDC)	30600		250	185
Benzene	ND		250	145
Trichloroethene	ND		250	115
1,2-Dichloropropane	ND	,	250	130
Bromodichloromethane	ND		250	115
2-Chloroethyl vinyl ether	ND		250	225
cis-1,3-Dichloropropene	ND		250	120
Toluene	ND		250	85.0
trans-1,3-Dichloropropene	ND		250	160
1,1,2-Trichloroethane	744		250	140
Tetrachloroethene	ND		250	110
Dibromochloromethane	ND		250	205
Chlorobenzene •	ND		250	135
	ND		250	130
Ethylbenzene	ND		500	330
Total Xylenes Bromoform	ND		250	225
	ND		250	215
1,1,2,2-Tetrachloroethane	ND ND		250	245
1,3-Dichlorobenzene	ND		250	245
1,4-Dichlorobenzene	ND		250	230
1,2-Dichlorobenzene	NL		200	•

Total Target Compounds (37):

35100

## **VOLATILE ORGANICS**

Lab ID: 09359-004 Client ID: M/C

Date Received: 09/14/2012 Date Analyzed: 09/18/2012

Data file: E5465.D

GC/MS Column: DB-624 Sample wt/vol: 0.05mL

Matrix-Units: Aqueous-μg/L (ppb)

Dilution Factor: 100 % Moisture: 100

Сотроинд	Concentration	Q	RL	MDL
Chloromethane	ND		50.0	49.0
Vinyl chloride	ND		50.0	32.0
Bromomethane	ND		50.0	49.0
Chloroethane	ND		50.0	40.0
Trichlorofluoromethane	ND		50.0	30.0
Acrolein	ND		1000	251
1,1-Dichloroethene	ND		50.0	28.0
Methylene chloride	ND		200	198
Acrylonitrile	ND		1000	181
tert-Butyl alcohol (TBA)	ND		100	69.0
trans-1,2-Dichloroethene	ND		50.0	23.0
Methyl tert-butyl ether (MTBE)	ND	*	50.0	27.0
1,1-Dichloroethane	ND		50.0	26.0
cis-1,2-Dichloroethene	ND	÷	50.0	26.0
Chloroform	2070		50.0	26.0
1,1,1-Trichloroethane	ND		50.0	27.0
Carbon tetrachloride	ND		50.0	27.0
1,2-Dichloroethane (EDC)	8190		50.0	37.0
Benzene	ND		50.0	29.0
Trichloroethene	ND		50.0	23.0
1,2-Dichloropropane	ND		50.0	26.0
Bromodichloromethane	ND		50.0	23.0
2-Chloroethyl vinyl ether	ND		50.0	45.0
cis-1,3-Dichloropropene	ND		50.0	24.0
Toluene	ND		50.0	17.0
trans-1,3-Dichloropropene	ND		50.0	32.0
1,1,2-Trichloroethane	416		50.0	28.0
Tetrachloroethene	ND		50.0	22.0
Dibromochloromethane	ND		50.0	41.0
Chlorobenzene	ND		50.0	27.0
Ethylbenzene	ND		50.0	26.0
Total Xylenes	ND		100	66.0
Bromoform	ND	•	50.0	45.0
1,1,2,2-Tetrachloroethane	ND		50.0	43.0
1,3-Dichlorobenzene	ND		50.0	49.0
1,4-Dichlorobenzene	ND		50.0	49.0
1,2-Dichlorobenzene	ND		50.0	46.0
,				

Total Target Compounds (37):

10700

## **VOLATILE ORGANICS**

Lab ID: 09359-005 Client ID: M/CONTROL Date Received: 09/14/2012

Date Analyzed: 09/25/2012

Data file: L3726.D

GC/MS Column: DB-624 Sample wt/vol: 0.01g

Matrix-Units: Soil-mg/Kg (ppm)

Dilution Factor: 500 % Moisture: 21.2

Compound	Concentration	Q	RL	MDL
Chloromethane	ND		0.635	0.146
Vinyl chloride	ND		0.635	0.419
Bromomethane	ND		0.635	0.349
Chloroethane	ND		0.635	0.266
Trichlorofluoromethane	ND		0.635	0.298
Acrolein	ND		12.7	1.51
1,1-Dichloroethene	ND		0.635	0.527
Methylene chloride	ND		1.27	1.26
Acrylonitrile	ND		12.7	0.996
tert-Butyl alcohol (TBA)	ND		1.27	0.463
trans-1,2-Dichloroethene	ND		0.635	0.324
Methyl tert-butyl ether (MTBE)	ND		0.635	0.178
1,1-Dichloroethane	ND		0.635	0.260
cis-1,2-Dichloroethene	ND		0.635	0.235
Chloroform	2.54		0.635	0.235
1,1,1-Trichloroethane	ND		0.635	0.298
Carbon tetrachloride	ND		0.635	0.451
1,2-Dichloroethane (EDC)	64.1		0.635	0.152
Benzene	ND		0.635	0.152
Trichloroethene	ND		0.635	0.305
1,2-Dichloropropane	ND		0.635	0.235
Bromodichloromethane	ND		0.635	0.197
2-Chloroethyl vinyl ether	ND		0.635	0.222
cis-1,3-Dichloropropene	ND		0.635	0.165
Toluene	ND		0.635	0.146
trans-1,3-Dichloropropene	ND		0.635	0.140
1,1,2-Trichloroethane	0.428	J	0.635	0.171
Tetrachloroethene	ND		0.635	0.317
Dibromochloromethane	ND		0.635	0.197
Chlorobenzene	ND		0.635	0.209
Ethylbenzene	ND		0.635	0.228
Total Xylenes	ND		1.27	0.438
Bromoform	ND	•	0.635	0.146
1,1,2,2-Tetrachloroethane	ND		0.635	0.152
1,3-Dichlorobenzene	ND	•	0.635	0,209
1,4-Dichlorobenzene	ND		0.635	0.178
1,2-Dichlorobenzene	ND		0.635	0.209
*				

Total Target Compounds (37):

67.1

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## VOLATILE ORGANICS

Lab ID: 09359-006 Client ID: M/A

Date Received: 09/14/2012 Date Analyzed: 09/25/2012

Data file: L3724.D

GC/MS Column: DB-624 Sample wt/vol: 0.05g

Matrix-Units: Soil-mg/Kg (ppm)

Dilution Factor: 100 % Moisture: 19.3

Compound	Concentration	Q	RL	MDL
Chloromethane	ND		0.124	0.029
Vinyl chloride	ND		0.124	0.082
Bromomethane	ND		0.124	0.068
Chloroethane	ND		0.124	0.052
Trichlorofluoromethane	ND		0.124	0.058
·	ND		2.48	0.295
Acrolein	ND		0.124	0.103
1,1-Dichloroethene	ND		0.248	0.245
Methylene chloride	ND		2.48	0.195
Acrylonitrile	ND		0.248	0.090
tert-Butyl alcohol (TBA)	ND		0.124	0.063
trans-1,2-Dichloroethene	ND		0.124	0.035
Methyl tert-butyl ether (MTBE)	ND		0.124	0.051
1,1-Dichloroethane	ND		0.124	0.046
cis-1,2-Dichloroethene	0.779		0.124	0.046
Chloroform	ND		0.124	0.058
1,1,1-Trichloroethane	ND		0.124	0.088
Carbon tetrachloride	16.7		0.124	0.030
1,2-Dichloroethane (EDC)	ND		0.124	0.030
Benzene	ND ND		0.124	0.060
Trichloroethene	ND ND		0.124	0.046
1,2-Dichloropropane	ND ND		0.124	0.038
Bromodichloromethane	ND ND		0.124	0.043
2-Chloroethyl vinyl ether	ND ND		0.124	0.032
cis-1,3-Dichloropropene	ND ND		0.124	0.029
Toluene			0.124	0.027
trans-1,3-Dichloropropene	ND		0.124	0.034
1,1,2-Trichloroethane	0.184		0.124	0.062
Tetrachloroethene	ND		0.124	0.038
Dibromochloromethane	ND		0.124	0.041
Chlorobenzene	ND		0.124	0.045
Ethylbenzene	ND		0.124	0.086
Total Xylenes	ND		0.124	0.029
Bromoform	ND	•	0.124	0.030
1,1,2,2-Tetrachloroethane	ND			0.041
1,3-Dichlorobenzene	ND		0.124	0.035
1,4-Dichlorobenzene	ND		0.124	0.033
1,2-Dichlorobenzene	ND		0.124	V.V71

Total Target Compounds (37):

17.7

## VOLATILE ORGANICS

Lab ID: 09359-007

Client ID: M/B

Date Received: 09/14/2012 Date Analyzed: 09/26/2012

Data file: F9206.D

GC/MS Column: DB-624

Sample wt/vol: 5g

Matrix-Units: Soil-mg/Kg (ppm)

Dilution Factor: 1 % Moisture: 17.5

	Concentration	n Q RL		MDL
Compound	ND		0.00121	0.000496
Chloromethane	ND		0.00121	0.000581
Vinyl chloride	ND		0.00121	0.000424
Bromomethane	ND		0.00121	0.000545
Chloroethane	ND		0.00121	0.000496
Trichlorofluoromethane	ND		0.024	0.00173
Acrolein	ND ND		0.00121	0.000605
1,1-Dichloroethene			0.00242	0.0024
Methylene chloride	ND		0.024	0.00227
Acrylonitrile	ND		0.00484	0.0011
tert-Butyl alcohol (TBA)	ND		0.00121	0.00052
trans-1,2-Dichloroethene	ND		0.00121	0.000278
Methyl tert-butyl ether (MTBE)	ND		0.00121	0.000327
1,1-Dichloroethane	ND			0.000327
cis-1,2-Dichloroethene	ND		0.00121	0.000373
Chloroform	ND		0.00121	0.000399
1,1,1-Trichloroethane	ND		0.00121	0.000399
Carbon tetrachloride	ND		0.00121	0.000450
1,2-Dichloroethane (EDC)	0.011		0.00121	0.000254
Benzene	ND		0.00121	0.00029
Trichloroethene	ND		0.00121	
1,2-Dichloropropane	ND		0.00121	0,000266
Bromodichloromethane	ND		0.00121	0.000387
2-Chloroethyl vinyl ether	ND		0.00121	0.000278
cis-1,3-Dichloropropene	ND		0.00121	0.000315
Toluene	ND		0.00121	0.000303
trans-1,3-Dichloropropene	ND		0.00121	0.000315
1,1,2-Trichloroethane	0,000502	J	0.00121	0.000242
Tetrachloroethene	ND		0.00121	0.000315
Dibromochloromethane	ND		0.00121	0.000266
	ND		0.00121	0.000266
Chlorobenzene	ND		0.00121	0.000375
Ethylbenzene	· ND		0.00242	0.00128
Total Xylenes	ND	•	0.00121	0.000387
Bromoform	ND		0.00121	0.000278
1,1,2,2-Tetrachloroethane	ND .		0.00121	0.000375
1,3-Dichlorobenzene	ND ND		0.00121	0.000375
1,4-Dichlorobenzene 1,2-Dichlorobenzene	ND ND		0.00121	0.000436
434 27404104 0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2				

Total Target Compounds (37):

0.012

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## **VOLATILE ORGANICS**

Lab ID: 09359-008

Client ID: M/C

Date Received: 09/14/2012 Date Analyzed: 09/26/2012

Data file: F9207.D

GC/MS Column: DB-624

Sample wt/vol: 5g

Matrix-Units: Soil-mg/Kg (ppm)

Dilution Factor: 1 % Moisture: 20.1

Compound	Concentration	Q	RL	MDL
Chloromethane	ND		0.00125	0.000513
Vinyl chloride	ND		0.00125	0.0006
Bromomethane	ND		0.00125	0.000438
Chloroethane	ND		0.00125	0.000563
Trichlorofluoromethane	ND		0.00125	0.000513
Acrolein	ND		0.025	0.00179
	ND		0.00125	0.000625
1,1-Dichloroethene	ND		0.0025	0.00248
Methylene chloride	ND		0.025	0.00235
Acrylonitrile	ND		0.005	0.00114
tert-Butyl alcohol (TBA)	ND		0.00125	0.000538
trans-1,2-Dichloroethene	ND		0,00125	0.000288
Methyl tert-butyl ether (MTBE)	ND ND		0.00125	0.000338
1,1-Dichloroethane	ND		0.00125	0.000388
cis-1,2-Dichloroethene	ND ND		0.00125	0.000363
Chloroform	ND		0.00125	0.000413
1,1,1-Trichloroethane	ND ND		0.00125	0,000513
Carbon tetrachloride	0,00632		0.00125	0,000263
1,2-Dichloroethane (EDC)	0,00032 ND		0.00125	0.0003
Benzene			0.00125	0.0004
Trichloroethene	ND		0.00125	0.000275
1,2-Dichloropropane	ND		0.00125	0.0004
Bromodichloromethane	ND		0.00125	0.000288
2-Chloroethyl vinyl ether	ND		0.00125	0.000325
cis-1,3-Dichloropropene	ŅD		0.00125	0,000313
Toluene	ND .		0.00125	0.000315
trans-1,3-Dichloropropene	ND			0.00025
1,1,2-Trichloroethane	0.000455	J	0.00125	0.00025
Tetrachloroethene	ND		0.00125	0.000325
Dibromochloromethane	ND		0.00125	0.000275
Chlorobenzene	ND		0.00125	
Ethylbenzene	ND		0.00125	0.000388
Total Xylenes	ND		0.0025	0.00133
Bromoform	ND		0.00125	0.0004
1,1,2,2-Tetrachloroethane	ND		0.00125	0.000288
1,3-Dichlorobenzene	ND		0.00125	0.000388
1,4-Dichlorobenzene	ND		0.00125	0.000388
1,2-Dichlorobenzene	ND		0.00125	0.00045

Total Target Compounds (37):

0.00678

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# Ferrous (II) Iron

# Client/Project; ISOTEC/PB&W/FORMOSA PLASTICS - 901132

Date Received: 09/14/12 17:30

,								%	
	Client ID	Result	o	DF	Matrix-Unit	MDL	RL	Solid	Date Analyzed
Lab ID	Client ID			1	Aqueous-ug/L	40.0	200	0	09/14/12 17:35
09359-001	M/CONTROL	ND		1	Aqueous-ug/L	40.0	200	0	09/14/12 17:35
09359-002	M/A	ND		1	· · · · · · · · · · · · · · · · · · ·	40.0	200	Ô	09/14/12 17:35
09359-003	M/B	ND		7	Aqueous-ug/L		200	Ŏ	09/14/12 17:35
09359-004	M/C	ND		1	Aqueous-ug/L	40.0	200	v	00/11/2 11/00



Integrated Analytical Labs 273 Franklin Road Randolph, NJ 07869 Contact Us: 973-361-4252

Fax: 973-989-5288

Web: www.lalonline.com

CUSTOMER INFO	REPORTI	NG INFO	Turnaround ?	ime (starts	the follow:	ng day if sampl	es rec'd	at lab > 5PM	)			6 % - 44	學為		AP(%) [45](1)
Company: ISOTEC-NJ	REPORT TO:	·				RUSH TAT prio						r Gi	JARA	NTEE	D)
Address:	Address:		ACCOMMO		XV Y ALLI	RUSHIBURC		, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		10L					
			PHC MUST	CHOOSI		eron Az filotophilosofi	. :	Rush TAT Charge *	Rej	port)	Format	$\perp$	E	DDs	
Telephone #:	Attn:		NJ EPH DRO (	day TAT)	NJ EPE	I Fractionated (5 da	YTAT)	<u>.</u>	R	esult	s Only	7	NJ SE	RP forms	at
Fax#:	FAX#		NJ EPH - C40 (	5 day TAT)				24 hr - 100%		Redi	aceđ		N	SDEC	
Project Manager: Prasad Kakarla	INVOICE TO:		DRO-8015 (3-5	day TAT)	QAI	M025 (5 day TAT )		48 hr - 75% 72 hr - 50%			ry - 15%			roved cus	stom
EMAIL Address:	Address:		Verbal/Fax:	Std 2 wk unle	ss otherwise	specified		96 hr - 35% 5 day - 25%	Sur	charg	ge applie	s	]	EDD	
Sampler: Yan Chin			24 hr**	18 hr**	72 hr**	96 hr**	l wk**	6-9 day 10%	Off	ıer (d	describe	) N	IO EDI	D/CD RE	EQ'D
Project Name: PB&W/Formosa Plas	tics	,	Other** (speci	fy):		7 A.V. of Arts artern arts (Francis and Arts and		<u> </u>					4		
Project Location (State):	Attn:		Hard Copy:	Std 3 week	<u>(*</u>	Other - call for	price	<del> </del>		<u></u>	Cooler Te	.mp	<u>_</u> _	°C	
Bottle Order #:	PO# 4258			4	ANALYT	ICAL PARAM	ETERS				# <i>BO</i>			_	
Quote #: 901132	Sample	Matrix	` '	2					1	<u>P</u>	RESE	RV	ATIV	<u>ES</u>	
	DW - Drinking Water AQ - Aquo		5.8	iron					١,	1		1	ş	1 [	
SAMPLE INFORMATION	OI - Oil LIQ - Liquid (Specify) S - Soil SL - Sludge SOL - Solid		2003	タニ							l as 1 ,	_	* .		a.
Client ID Depth (ft only)	Sampling Date Time	Matrix # IA	L# > 1	-4-					HCL	HINO3	MeOH	HON	Oiber Oiber	None	Enco
M/Control	9/14/12	AQ I+1	X	×					1	<u> </u>		_		(	
M/A			2	Х					1	<u></u>		$\perp$			
M/B			3	X					1	<u> </u>	igspace	$\downarrow$		1	
MIC		V V 4		X			_			ــــــ	<del>                                     </del>	_		1_	
MICOntrol		5 1 5	5						ļ	ļ	$\perp \perp$	4		1	
MIA		1 6								ऻ_	1	4	$\perp$	1	
M/B		7						ļ	<u> </u>	<u> </u>		$\downarrow$			
M/C	V	V V 8						<u> </u>		<u>L</u>				]	
Known Hazard: Yes or No Describe:	Conc. Expected: Low M					- SRS - SRS/IGW			R (SE	E CC	)MMEI	NTS	<u>,                                     </u>		
Please print legibly and fill out completely. S	Samples cannot be proc	essed and the turnaro	und time Will	not start i	u <b>n</b> tii any	amoiguities n	ave peer	n resoivea.	Cor	. <del>]</del> v	ام		•		
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Signature/Company	Date Time	Signature/Com	Bany		Date	Time		nents: USE	54j	ادع			-51	1020	
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01/2012 rev

## PROJECT INFORMATION



Case No.	12-09359 Project	PB&W/FORMOSA	PLASTICS - 901132
Customer	Isotec		P.O. # 4258
Contact EMail Phone	Prasad Kakarla pkakarla@insituoxidation.com; ychin@insituoxidation.com (609) 275-8500 Fax 1(60	☑ EMail EDDs 09) 275-9608	Received 9/14/2012 17:30  Verbal Duc 10/1/2012  Report Duc 10/8/2012
Report To 11 Princess Suite A	Road iile, NJ 08648		Bill To 11 Princess Road Suite A Lawrenceville, NJ 08648 Attn: Prasad Kakaria
Report I		Field Sampling	Conditional VOA

09359-003 M/B 09359-004 M/C 09359-005 M/CONTROL	Depth Top / Bottom n/a n/a n/a n/a n/a n/a n/a n/a n/a n/a	Sampling Time 9/14/2012 9/14/2012 9/14/2012 9/14/2012 9/14/2012 9/14/2012 9/14/2012 9/14/2012	Aqueous Aqueous Soil Soil	ug/L ug/L ug/L ug/L mg/Kg	2
Sample # Tests	Status Q In Process 624	A Method			
001 PP VO + Cis 1,2-DCE + MTBE TBA  " Ferrous (II) Iron		r 120 3500 Fe B			
AND DRIVING A Cir. 1.2-DCF + MTRE TRA	In Process 624	1			
Ferrous (II) Iron	Run SM	120 3500 Fe B			
003 PP VO + Cis 1.2-DCE + MTBE _TBA	In Process 62	1			
4.00 14.0	Run SN				
2 Table 11 Sept. 11 Sept. 2014		120 3500 Fe B			
005 PP VO + Cis 1,2-DCE + MTBE_TBA		60B			
006 PPNO + Cis 1,2-DCE + MTBE_TBA	Run 82	60B			
007 PP VO + Cis 1,2-DCE + MTBE_TBA 008 PP VO + Cis 1,2-DCE + MTBE_TBA		60B · 154			

#### 09/17/2012 10:22 by Ellen - NOTE I

USE LOWEST POSSIBLE MDLs. MDLs FOR CONTROL SAMPLES SHOULD NOT BE LOWER THAN MDLs FOR OTHER SAMPLES.

## PROJECT INFORMATION



Case No. E12-09359

Project PB&W/FORMOSA PLASTICS - 901132

09/17/2012 16:37 by Mark - NOTE 2

SAMPLES #005 - 008 HAVE SOIL LAYER & WATER LAYER. PER YAN CHEN, ANALYZE SOIL LAYER ONLY

E12-09359

# SAMPLE RECEIPT VERIFICATION

CASE NO: E 12 09359 CLIENT:
COOLER TEMPERATURE: 2° - 6°C:✓ (See Chain of Custody)  Comments
COC: COMPLETE KEY
<ul> <li>✓ Bottles Intact</li> <li>✓ no-Missing Bottles</li> <li>✓ no-Extra Bottles</li> </ul>
✓ Sufficient Sample Volume  ✓ no-headspace/bubbles in VOs  ✓ Labels intact/correct  ✓ pH Check (exclude VOs) <sup>1</sup>
✓ Correct bottles/preservative ✓ Sufficient Holding/Prep Time'
Sample to be Subcontracted  ✓ Chain of Custody is Clear
All samples with "Analyze Immediately" holding times will be analyzed by this laboratory past the holding time. This includes but is not limited to the following tests: pH, Temperature, Free Residual Chlorine, Total Residual Chlorine, Dissolved Oxygen, Sulfite.  ADDITIONAL COMMENTS:  SAMPLE(S) VERIFIED BY: INITIAL DATE 9 14/12  CORRECTIVE ACTION REQUIRED: YES SEE BELOW)
If COC is NOT clear, <u>STOP</u> until you get client to authorize/clarify work.
CLIENT NOTIFIED: PROJECT CONTACT: SUBCONTRACTED LAB: DATE SHIPPED: ADDITIONAL COMMENTS:
VERIFIED/TAKEN BY: INITIAL DATE GUAL E12-238日32009 到到1

# Laboratory Custody Chronicle

IAL Case No.

E12-09359

Client Isotec

Project PB&

PB&W/FORMOSA PLASTICS - 901132

Received On 9/14

9/14/2012@17:30

Department: Volatiles PP VO + Cis 1,2-DCE + MTBE & TBA		Aqueous  " " Soil " "	Prep. Date n/a n/a n/a n/a n/a n/a n/a n/a n/a n/a	Analyst n/a n/a n/a n/a n/a n/a n/a n/a n/a n/a	Analysis Date 9/17/12 9/17/12 9/17/12 9/18/12 9/25/12 9/25/12 9/26/12	Analyst Barbara Barbara Barbara Barbara Mei Mei Xing Xing
Department: Wet Chemistry Ferrous (II) Iron	-001 -002 -003 -004		Prep. Date n/a n/a n/a n/a	Analyst n/a n/a n/a n/a n/a	Analysis Date 9/14/12@17:35 9/14/12@17:35 9/14/12@17:35 9/14/12@17:35	Analyst Kris Kris Kris Kris



# ANALYTICAL DATA REPORT

Isotec 11 Princess Road Suite A Lawrenceville, NJ 08648

Project Name: PB&W/FORMOSA PLASTICS - 901132

IAL Case Number: E12-09628

These data have been reviewed and accepted by:

Michael H. Lefth, Ph.D.

Laboratory Director

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# Sample Summary

IAL Case No.

E12-09628

Client Isotec

Project PB&W/FORMOSA PLASTICS - 901132

Received On 9/21/2012@18:45

					<u># of</u>
Lab ID	Client Sampl <u>e ID</u>	Depth Top/Bottom	Sampling Time	<u>Matrix</u>	<u>Container</u>
09628-001	S-A/CONTROL AQUEOUS SAMPI	n/a	9/21/2012@13:00	Aqueous	1
09628-002	S-A/A AQUEOUS SAMPLE	n/a	9/21/2012@13:00	Aqueous	1
09628-003	S-A/B AQUEOUS SAMPLE	n/a	9/21/2012@13:00	Aqueous	1
09628-004	S-A/C AQUEOUS SAMPLE	n/a	9/21/2012@13:00	Aqueous	1
09628-005	S-H/CONTROL AQUEOUS SAMPI	n/a	9/21/2012@13:00	Aqueous	1
09628-006	S-H/A AQUEOUS SAMPLE	n/a	9/21/2012@13:00	Aqueous	1
09628-007	S-H/B AQUEOUS SAMPLE	n/a	9/21/2012@13:00	Aqueous	1
09628-008	S-H/C AQUEOUS	n/a	9/21/2012@13:00	Aqueous	1
09628-009	S-A/CONTROL SOIL SAMPLE	n/a	9/21/2012@13:00	Soil	1
09628-010	S-A/A SOIL SAMPLE	n/a	9/21/2012@13:00	Soil	1
09628-011	S-A/B SOIL SAMPLE	n/a	9/21/2012@13:00	Soil	1
09628-012	S-A/C SOIL SAMPLE	n/a	9/21/2012@13:00	Soil	I
09628-013	S-H/CONTROL SOIL SAMPLE	n/a	9/21/2012@13:00	Soil	1
09628-014	S-H/A SOIL SAMPLE	n/a	9/21/2012@13:00	Soil	1
09628-015	S-H/B SOIL SAMPLE	n/a	9/21/2012@13:00	Soil	I
09628-016	S-H/C SOIL SAMPLE	n/a	9/21/2012@13:00	Soil	1
33 <b>5</b>					

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This are turn finalized on October 12, 2012	

<sup>\*</sup> Methodology is included in the IAL Project Information Page

#### **DEFINITIONS / QUALIFIERS**

## DATA QUALIFIERS

- **B** Indicates the analyte was found in the associated method blank as well as in the sample. It indicates probable laboratory contamination.
- C Indicates analyte is a common laboratory contaminant.
- <u>D</u> Indicated analyte was reported from diluted analysis.
- **E** Identifies a compound concentration that exceeds the upper level of the calibration range of the instrument for that specific analysis.
- <u>J</u> Indicates an estimated value. This flag is used when the concentration in the sample is below the RL but above the MDL.

## REPORTING DEFINITIONS

- RL Reporting Limit. The RL is determined by the lowest concentration in the calibration curve. For most Wet Chemistry methods, the RL is defined by using the PQL.
- MDL Method Detection Limit as determined according to 40CFR Part 136 Appendix B.
- PQL Practical Quantitation Limit. Usually defined as a value 3-5 times the MDL.
- ND Indicates analyte was analyzed for but not detected above the MDL.
- **DF** Dilution Factor
- **LCS** Laboratory Control Sample
- **LCSD** Laboratory Control Sample Duplicate
  - MS Matrix Spike
  - MSD Matrix Spike Duplicate
- **DUP** Duplicate